NASA Contractor Report 189618

N-05 P-75 127091

1990 High-Speed Civil Transport Studies

HSCT Concept Development Group Advanced Commercial Programs

McDonnell Douglas Corporation Douglas Aircraft Company Long Beach, California

Contract NAS1-18378 October 1992

(NASA-CR-189618) THE 1990 HIGH-SPEED CIVIL TRANSPORT STUDIES Final Report, 1 Oct. 1989 - 31 Mar. 1991 (McDonnell-Douglas Corp.) 75 p

N93-16947

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G3/05 0127091

National Aeronautics and

Space Administration

Langley Research Center Hampton, Virginia 23665-5225 <u>\$</u>'

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1990 HIGH-SPEED CIVIL TRANSPORT STUDIES

HSCT CONCEPT DEVELOPMENT GROUP ADVANCED COMMERCIAL PROGRAMS

DOUGLAS AIRCRAFT COMPANY LONG BEACH, CA 90846

CONTRACT NAS1-18378

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ABSTRACT

This report contains the results of the Douglas Aircraft Company system studies related to high-speed civil transports (HSCTs). The tasks were performed under an 18-month extension of NASA Langley Research Center Contract NAS1-18378.

The system studies were conducted to assess the emission impact of HSCTs at design Mach numbers ranging from 1.6 to 3.2. The tasks specifically addressed an HSCT market and economic assessment, development of supersonic route networks, and an atmospheric emissions scenario.

The general results indicated (1) market projections predict sufficient passenger traffic for the 2000 to 2025 time period to support a fleet of economically viable and environmentally compatible HSCTs; (2) the HSCT route structure to minimize supersonic overland traffic can be increased by innovative routing to avoid land masses; and (3) the atmospheric emission impact on ozone would be significantly lower for Mach 1.6 operations than for Mach 3.2 operations.

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FOREWORD

The 1990 High-Speed Civil Transport Study was an 18-month extension of the previous 3 years' work (Phases I to IIIA). The 1990 systems studies evaluation covered the period from 1 October 1989 to 31 March 1991.

Work was accomplished as a task order activity by Douglas Aircraft Company in Long Beach, California. This work was under the direction of the NASA Langley Research Center, Hampton, Virginia, and was funded under Contract NAS1-18378.

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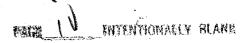
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CONTENTS

Section		age
1	SUMMARY	1
2	INTRODUCTION	3
3	MARKET AND ECONOMIC ASSESSMENT 3.1 Traffic Projection 3.2 Fleet Requirement 3.3 Cash Operating Cost Comparison 3.3.1 Revenue 3.3.2 Operating Costs 3.3.3 Operating Profit 3.3.4 Aircraft Worth 3.3.5 Conclusion and Further Studies	5 8 13 13 13 14 15 15
4	SUPERSONIC NETWORK EVALUATION 4.1 Aircraft Economic Performance 4.1.1 Time Savings 4.1.2 Operating Cost and Profit 4.1.3 Aircraft Worth	17 18 18 18 19
	4.1.4 Fare Premium 4.2 Supersonic Network Scenarios 4.2.1 Methodology 4.2.2 Route Diversion Analysis 4.2.3 Overwater Network Scenario 4.3 Conclusion	21 22 22 24 27 28 28
5	4.4 Recommendations for Further Study ATMOSPHEIRC EMISSIONS IMPACT STATUS 5.1 Brief Methodology Review 5.2 Atmospheric Emission Scenarios 5.3 Ozone Impact Trade Studies 5.4 Cruise Altitude Restrictions 5.5 Conclusions 5.6 Future Plans and Recommendations	33 33 34 36 39 44 45
6	CONCLUSIONS	47
7	RECOMMENDATIONS	49
PPENDE	A - Basic Traffic Data Base, 250 City-Pairs in Descending Order of Scheduled Seats	A- 1
	B - Great Circle Versus Diverted Distances, Strip Charts for Top 20 City-Pairs	B-1
APPENDE	C Ground Track Profile Display, 250 City-Pairs	C-1

			,	
				÷,

ILLUSTRATIONS

Figure		Page
3-1	Douglas Mach 1.6 Turbulent Baseline Configuration, D1.6-3	6
3-2	Douglas Mach 2.2 Turbulent Baseline Configuration, D2.2-10	6
3-3	Douglas Mach 3.2 Turbulent Baseline Configuration, D3.2-7A	7
3-4	International Passenger Traffic — Major Regions (85-90 Percent of Total)	7
3-5	Distribution of Annual Seat-Miles for Major 10 Regions for Year 2000	. 8
3-6	Passenger Aircraft Capacity/Supply Forecast	9
3-7	Passenger Capacity Trends by Generic Class	9
3-8	Commercial Passenger Jetliners in Year 2000	10
3-9	Generic Passenger Aircraft Requirements in Year 2000	11
3-10	Generic Passenger Aircraft Requirements Including Supersonic Class in Year 2000	11
3-11	Projected HSCT Demand in Year 2000 as a Function	
	of Fare Premium Levels	
3-12	Operating Cost Breakdown — No Ownership-Related Costs	
3-13	Operating Performance (Revenue – Cost = Profit)	
4-1	Time Performance	
4-2	Operating Performance	19
4-3	Economic Performance Percentage of Operating Cost	•
	and Profit to Revenue	
4-4	HSCT Miles per 1,000 Pounds of Fuel at 4,500 n mi	
4-5	Effect of Overland Off-Design Operation on Aircraft Worth	
4-6	Time Savings and Trip Price Relationship	22
4-7	Supersonic Network Scenarios for Unrestricted and	23
	Restricted Operation	
4-8	Traffic Analysis by IATA Regions	
4-9	Top 250 Potential Supersonic Routes (No Restrictions)	
4-10	City-Pair Evaluation — JFK (New York)-LHR (London)	
4-11	Diverted Routing — New York-Tokyo	
4-12	HSCT Top Seat Rank 250 Airport-Pairs	
4-13	HSCT Top Seat Rank 150 Airport-Pairs	
4-14	100 City-Pairs for Overwater Only — Supersonic Network	
4-15	Supersonic Network Scenario for 200 City-Pairs	
5-1	HSCT Representative City-Pairs	34
5-2	Data Flow for Generating Inputs to Global Atmospheric Models	
5-3	Ozone Depletion by Year — P&W TBE Engine	37
5-4	Ozone Depletion Versus Engine Type — Mach 3.2	37

			ik .
Figure		Page	
5-5	Ozone Depletion and Fleet Size Versus Number of Flights for P&W TBE	38	
5-6	Fare Premium Impact on Ozone Concentration	39	
5-7	Cruise Altitude Restriction Ozone Impact		,
5-8	Effects of Cruise Altitude Restriction on MTOGW and Range — Mach 3.2	41	
5-9	Effect of Cruise Altitude Restriction on Market Capture (Annual Seat-Miles)		•
5-10	Effect of Cruise Altitude on Operating Performance — Mach 3.2	42	
5-11	Effect of Cruise Altitude Restrictions on Operating Cost and Profit — Mach 3.2	43	
5-12	Effect of Cruise Altitude Restriction on Operating Cost and Fuel Cost — Mach 3.2 Without Resizing	43	
5-13	Effect of Cruise Altitude on Aircraft Worth and Operating Profit — Mach 3.2 Without Resizing	44	
5-14	Effect of Cruise Altitude Restrictions on Aircraft Worth After Commencement of Production (Without Resizing)	45	

TABLES

Table		Page
3-1	Fleet Projections Based on HSCT Demand	12
3-2	Revenue for Mach 1.6, 2.2, 3.2 Aircraft	13
3-3	Annual Revenue per Aircraft	
3-4	Operating Cost Data for Mach 1.6, 2.2, 3.2 Aircraft	14
3-5	Annual Cash Flow per Aircraft	15
3-6	Aircraft Worth at 10-Percent ROI	16
4-1	Example of Ground Track Profile Display for New York-Tokyo	28
5-1	Total Annual Fuel Burn by Region	36
5-2	NO. Emission Indices for Various Engine Concepts	36
5-3	Aircraft Economic Performance at Different Cruise Altitudes	44

SECTION 1 SUMMARY

The 1990 system study report contains technical, environmental, marketing, and economic assessments; discusses issues and concerns; and makes recommendations for further system studies. This report focuses on the atmospheric emission impact, marketing, and economic aspects of the HSCT. It contains results of a Douglas Aircraft Company study to evaluate the commercial viability of the HSCT. The approach was to evaluate, under simulated airline operations, worldwide market demand, fleet requirements, realistic supersonic route structures, and HSCT economic performance. Subsequently, atmospheric emission scenarios were developed, and emission impact was evaluated for three Mach number configurations — 1.6, 2.2, and 3.2.

Market and Economic Assessments — Traffic projections for the years 2000 to 2025 and fleet requirements over a Mach number range of 1.6 to 3.2 have been assessed with regard to Mach number, fare premium, and aircraft range. At Mach 2.2, fleet needs could total 2,300 or more 300-seat aircraft by the year 2025. The prime conditions for economic viability include (1) airplane revenues covering operating costs plus an attractive rate of return to the operator, (2) fares compatible with the subsonic fleet to expand HSCT service, and (3) a market large enough to permit a selling price lower than the investment value of the airplane.

Supersonic Network Evaluation — Only a few candidate global airline network scenarios for HSCT have been assembled. The high-density long-range markets were selected from the Official Airline Guide (OAG) on-line data base. Creative rerouting was conducted to minimize overland segments and to lessen the impact of the environmental restrictions that may be imposed on future supersonic operation.

The data on these network scenarios represent an assembly of global routes from which HSCT global traffic networks can be constructed. The network scenarios provide examples on how supersonic service may bring some changes to the current global route structure. Some of these supersonic network scenarios show good potential of capturing more than half the market share of the long-range traffic.

Atmospheric Emissions Impact Status — An engine emission annual fuel burn model was developed for input to 20 atmospheric models. Atmospheric emission scenarios were produced for three HSCT configurations at Mach 1.6, 2.2, and 3.2 The atmospheric global model results showed that ozone depletion is a function of the aircraft's cruise Mach number primarily because of the strong dependence of ozone impact on injection altitude. The atmospheric impact of ozone depletion of the Mach 1.6 configuration is considerably less than that of the Mach 2.2 and 3.2 configurations for a given combustor technology. The introduction of cruise altitude restrictions after the HSCT enters service could alleviate the ozone impact of the Mach 1.6 and 2.2 configurations. At Mach 3.2, however, the increased fuel burn more than offsets the advantage of lower injection altitude. All configurations will suffer some economic performance penalties if forced below their optimum operating cruise altitude.

SECTION 2 INTRODUCTION

This report presents the results of Douglas HSCT system studies. It is a continuation of environmental and economic studies completed in the 1989 system study. In this report, market projections have been made for the years 2000 to 2025, fleet requirements have been assessed over a Mach number range of 1.6 to 3.2, and a number of supersonic network scenarios have been evaluated.

Additionally, for atmospheric studies, engine emissions have been developed into annual emission fuel burn constituents to provide input data to an atmospheric impact two-dimensional model.

SECTION 3 MARKET AND ECONOMIC ASSESSMENT

NASA Report 4235, submitted by Douglas at the conclusion of the Phase III studies, included an initial screening from Mach 2 to Mach 25, followed by a focus on the Mach 2 to Mach 5 range, as well as a comparison of Mach 3.2 and Mach 5.0. The economic potential for a high-speed commercial transport with respect to technical readiness, market characteristics, aviation infrastructure, and environmental issues was described. A forecast of air travel passengers indicated a need for HSCT service in the 2000-2025 time frame, conditioned on economic viability and environmental compatibility. Design requirements for this study focused on a 300-passenger, three-class aircraft with a range of 6,500 nautical miles, based on accelerated growth predictions for the Pacific region. Aircraft productivity was a key parameter, with aircraft worth in comparison to aircraft price being the airline-oriented figure of merit.

As a follow-up on previous studies, research for Task 11 has focused on three configuration designs: Mach 1.6, 2.2, and 3.2. An economic analysis of supersonic operation based on aircraft specifications has been conducted. The market research reflects refinements in market assumptions and projections, a better understanding of market elasticity and stimulation, the latest preliminary estimates for fleet requirements, the sensitivity of aircraft performance and economics to environmental constraints, and an updated parametric analysis of different design range and passenger configurations. This section covers traffic projection, fleet assessment, and an economic comparison of the three configuration designs at Mach 1.6, 2.2, and 3.2.

Three-view drawings of the baseline configurations used in the 1990 system studies for various environmental and economic studies are shown in Figures 3-1, 3-2, and 3-3. The development of these configurations was based on earlier phases of the current Douglas HSCT system study contract and on the Douglas Advanced Supersonic Transport (AST) activities of the 1970s. The fuselage was designed to accommodate 300 passengers in a nominal seating arrangement of three classes: 10, 30, and 60 percent for first, business, and coach classes, respectively. HSCT performance was analyzed according to commercial domestic and international rules and practices. The HSCT design range was 6,500 nautical miles in an all-supersonic cruise condition.

3.1 TRAFFIC PROJECTION

Traffic projection initially encompassed all international air traffic in 18 International Air Transport Association (IATA) regions. The 10 regions considered to be the best potential for supersonic operation were then studied in more detail. The air traffic forecasts prepared for the 10 regions were based on econometric models that relate traffic to national income, fares, yield, and, where appropriate, other relevant variables. Four of the 10 regions comprise about 85 percent of the total international traffic. Rapid economic growth in the Pacific-Asia region has made this the fastest growing area for passenger traffic. Figure 3-4 shows that North and Mid-Pacific traffic will equal North Atlantic traffic by the year 2000.

Long-term prospects for international passenger traffic gains are relatively good. Overall, traffic is predicted to total about 450 billion annual seat-miles (ASMs) by the year 2000 and

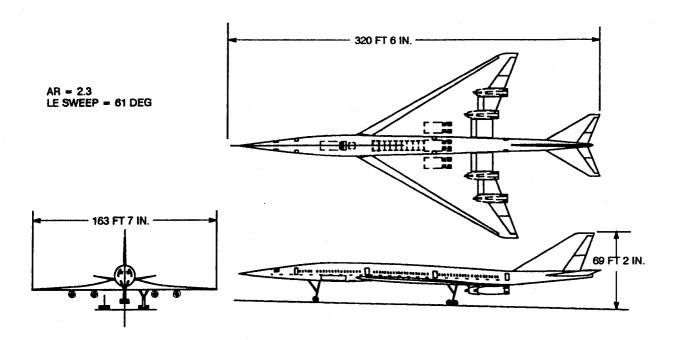


FIGURE 3.-1. DOUGLAS MACH 1.6 TURBULENT BASELINE CONFIGURATION, D1.6-3

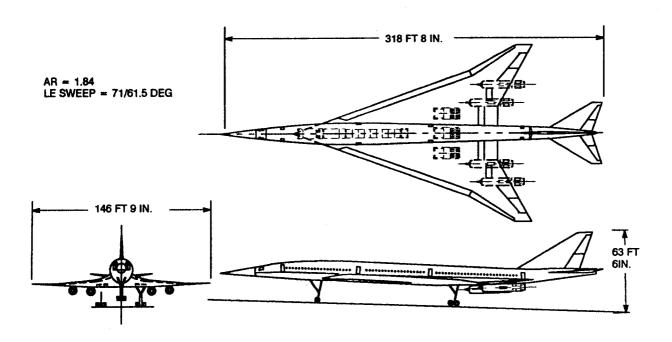


FIGURE 3-2. DOUGLAS MACH 2.2 TURBULENT BASELINE CONFIGURATION, D2.2-10

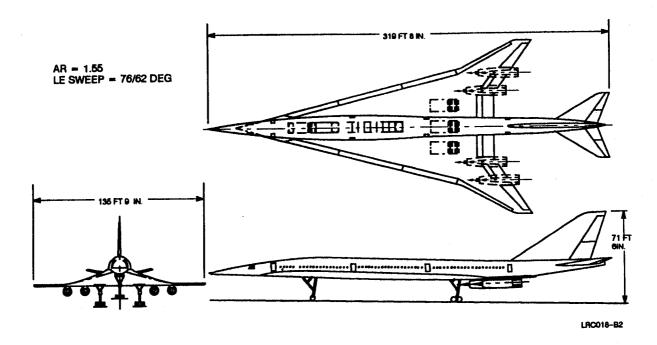


FIGURE 3-3. DOUGLAS MACH 3.2 TURBULENT BASELINE CONFIGURATION, D3.2-7A

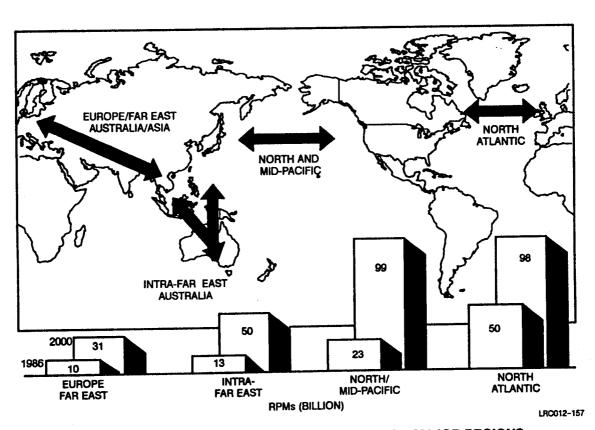


FIGURE 3-4. INTERNATIONAL PASSENGER TRAFFIC - MAJOR REGIONS (85-90 PERCENT OF TOTAL)

2.4 trillion ASMs by the year 2025, or five times the traffic projected for the year 2000. Figure 3-5 shows the distribution of the year 2000's ASMs among the 10 HSCT regions.

3.2 FLEET REQUIREMENT

In order to assess world HSCT fleet requirements, one has to examine the outlook for the commercial aviation industry as a whole. Traffic forecasts, economic parameters, current and future airlines fleet composition, and political trends and regulations must be monitored and analyzed to produce the most reliable projections for world supersonic fleet estimates. Projections of the future subsonic fleet, airline orders for firm and conditionally firm new aircraft, and retirement of the current fleet are among the primary considerations in assessing tomorrow's supersonic fleet.

The passenger traffic estimates, combined with load factor forecasts, produce the total capacity required in terms of available seat-kilometers, as indicated by the top line in Figure 3-6. With a long-term average capacity growth requirement forecast of 5.5 percent, nearly 4.5 trillion available seat-kilometers (ASKs) will be needed by the year 2000 to support the anticipated traffic level. Capacity provided by the current fleet will fall by 50 percent to 1 trillion ASKs in 2000 because of aircraft retirements. Partially offsetting this loss, however, is an additional 800 billion annual ASKs that will be provided by aircraft currently on order. The differential between the total capacity required and that supplied by the current fleet plus aircraft on order represents the capacity gap. This deficiency, which grows to 2.8 trillion ASKs by 2000, will be satisfied by new orders of generic aircraft. The size and range characteristics of the new aircraft required to fill the capacity gap are shown in Figure 3-7.

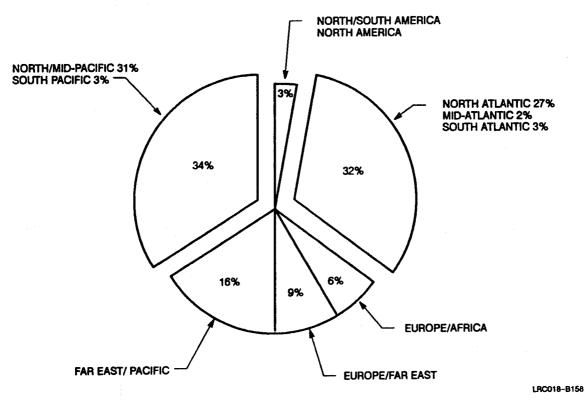


FIGURE 3-5. DISTRIBUTION OF ANNUAL SEAT-MILES FOR MAJOR 10 REGIONS FOR YEAR 2000

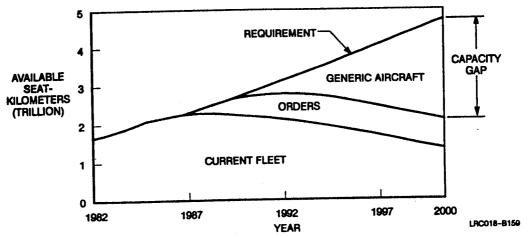


FIGURE 3-6. PASSENGER AIRCRAFT CAPACITY/SUPPLY FORECAST

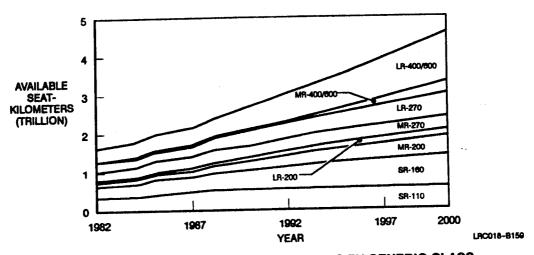


FIGURE 3-7. PASSENGER CAPACITY TRENDS BY GENERIC CLASS

Increased capacity will be demanded for all generic aircraft classes. However, it is significant that certain classes will outperform others on a relative basis. Inherent in the forecast is the fact that both airport and airspace congestion will force carriers to rely increasingly on larger aircraft instead of increased frequencies to satisfy projected traffic demands. Airlines will also rely on aircraft with higher productivity, such as the HSCT, to reduce congestion.

Airline transitions from subsonic aircraft to supersonic will also have an impact on the number of generic aircraft in the medium- and long-range categories. Productivity gains necessary to achieve the 5.5-percent worldwide average ASK escalation will be realized by changes in four components: aircraft units, average seat counts, utilization, and speed. An increase in aircraft units will be the dominant element in increasing ASKs. As larger transports replace smaller ones, the average seat count per aircraft will contribute to productivity gains. A relatively subordinate role will be played by aircraft utilization and increased flight speed unless the HSCT becomes available for commercial airlines. HSCT productivity gain due to speed will then become the dominant component, replacing aircraft units. It is conceivable that productivity gain may ultimately cause a decline in fleet size.

The growth in the world's airline industry will necessitate changes in the number and type of aircraft that serve it. Overall, the 6,500 passenger aircraft operated commercially by the late 1980s will advance to a world fleet approximating 10,000 airliners by the year 2000, a 54-percent unit increase. The dominant position of the short-range fleet will moderate as it falls to 56 percent of the world fleet in 2000 from its present 68-percent unit share. The medium- and long-range fleets will generate a significant relative unit gain over the forecast period.

The 10,000 commercial passenger jetliners forecast for the worldwide fleet in 2000 will be presented by a cross section of aircraft currently in service, transports presently on order, and projected new generic aircraft. Much of today's fleet will still be operating in commercial service by 2000. As shown in Figure 3-8, approximately 28 percent of the fleet in the year 2000 will be composed of units currently in service. The remainder of this fleet will be composed of jets currently on order (17 percent of the year 2000 fleet) and the projected new generic equipment (55 percent).

World demand for new passenger aircraft for the year 2000 is forecast at 5,500 units in addition to those currently on order. Figure 3-9 shows the generic passenger aircraft requirement by class. The medium- and long-range classes (greater than 3,500-nautical-mile range and 250 passengers) are expected to total more than 1,800 aircraft. Approximately one-half of this market is represented by the 10-region HSCT arena. Therefore, the HSCT with no fare premium may replace a maximum of 900 aircraft. At Mach 2.2, the HSCT is twice as productive as a subsonic aircraft of the same size. A fleet of approximately 450 HSCTs can transport the payload of 900 subsonic aircraft. Figure 3-10 shows the generic passenger aircraft requirements, including the HSCT, in the year 2000.

As supersonic speed changes, productivity changes as well, resulting in variations in fleet projections. Fleet requirements are sensitive to fare elasticity. Introduction of fare premiums will reduce fleet sizes. Table 3-1 shows HSCT fleet requirements at different fare premiums for the Mach 1.6, 2.2, and 3.2 configurations. It illustrates how fleet sizes are reduced as fare premiums increase. HSCT needs shown in the table cover the period from the year 2000 to the

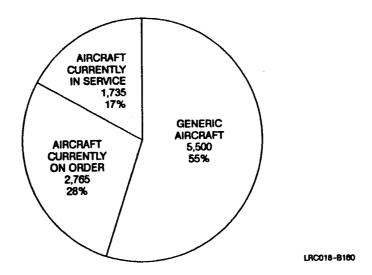


FIGURE 3-8. COMMERCIAL PASSENGER JETLINERS IN YEAR 2000

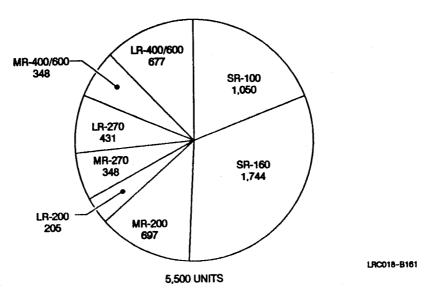


FIGURE 3-9. GENERIC PASSENGER AIRCRAFT REQUIREMENTS IN YEAR 2000

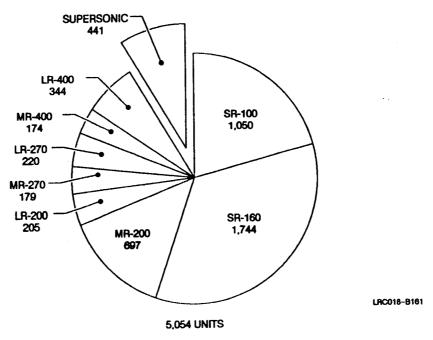


FIGURE 3-10. GENERIC PASSENGER AIRCRAFT REQUIREMENTS INCLUDING SUPERSONIC CLASS IN YEAR 2000

year 2025. Since there would be no HSCT aircraft in the commercial fleet as early as the year 2000, the subsonic fleet will continue to serve world traffic demands until the HSCT is introduced. If production rates are no greater than the rate of traffic growth, production quantities can be absorbed without premature retirement of the subsonic fleet. Figure 3-11 gives fleet projections for the year 2000.

Future fleet assessments need to examine some of the more complex factors that affect fleet projections. A better understanding of elasticity, stimulation, value of time, and fare premium

TABLE 3-1 FLEET PROJECTIONS BASED ON HSCT DEMAND

		NUMBER OF AIRCRAFT								
FARE PREMIUM LEVELS (PERCENT)	MACH 1.6		MACH 2.2		MACH 3.2					
	YEAR 2000	YEAR 2025	YEAR 2000	YEAR 2025	YEAR 2000	YEAR 2025				
0	521	2,725	441	2,315	365	1,954				
10	368	1,954	358	1,870	314	1,700				
20	201	1,097	230	1,194	210	1,147				
30	79	450	124	666	137	765				
40	34	198	57	314	74	423				
50	15	92	29	158	38	220				

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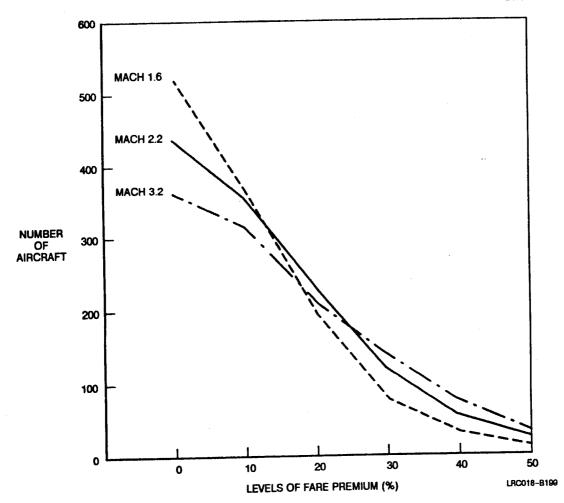


FIGURE 3-11. PROJECTED HSCT DEMAND IN YEAR 2000 AS A FUNCTION OF FARE PREMIUM LEVELS

will be reflected in fleet analyses. If supersonic cruise overland is restricted, fleet requirements will be reduced. The effect of such environmental restrictions as overland operation, cruise altitude, and emission index on supersonic fleet scenarios will be investigated.

3.3 CASH OPERATING COST COMPARISON

For a profitable supersonic operation, the airplane must generate enough revenue to cover its operating costs plus an attractive rate of return to the airlines. This section summarizes the results of the cash operating cost analysis and the commercial value of the three baseline configuration designs at Mach 3.2, 2.2, and 1.6. This evaluation examines the revenue side of the equation, followed by the operating cost, in order to arrive at the operating profit.

3.3.1 Revenue

Passenger revenue is based on published International Civil Aviation Organization (ICAO) fare data, fare premium assumptions, and corresponding HSCT market share statistics. Table 3-2 presents the revenue data for Mach 3.2, 2.2, and 1.6 configurations. As fare premiums increase, the HSCT market share is reduced. Revenue is improved because fares increase and the onboard passenger mix changes to favor the higher yield business- and first-class passengers. Table 3-3 illustrates the differences in revenue generating capabilities of Mach 3.2, 2.2, and 1.6 designs at various fare premiums.

3.3.2 Operating Costs

Cash operating cost studies were conducted to compare the relative operating cost of the Mach 3.2, 2.2, and 1.6 configurations, following the CAB Form 41 format for direct and indirect cash costs. Form 41 covers (1) flying operations, (2) maintenance, (3) passenger service, (4) aircraft and traffic servicing, (5) promotion and sales, and (6) general and administrative. Cost estimates were computed using Douglas operating cost formulas. Input data

TABLE 3-2
REVENUE FOR MACH 1.6, 2.2, 3.2 AIRCRAFT

		MACH 1.6	MACH 2.2	MACH 3.2
REVENUE PER SEAT-MILE	(\$)	0.072	0.073	0.073
REVENUE PER MILE	(\$)	21.81	21.93	21.95
REVENUE PER BLOCK HOUR	(\$)	20,285	25,610	33,473
REVENUE PER TRIP	(\$)	91,033	91,493	91,213
REVENUE PER AIRCRAFT PER YEAR	(\$)	63.31 MILLION	75.16 MILLION	91.31 MILLION

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TABLE 3-3
ANNUAL REVENUE PER AIRCRAFT
(\$ MILLION)

FARE PREMIUM (PERCENT)	MACH 1.6	MACH 2.2	MACH 3.2
0	63.31	75.16	91.31
10	78.20	88.10	105.72
20	93.41	104.62	128.92
30	113.64	121.16	146.54
40	131.98	144.63	169.28
50	137.59	165.75	198.61

included (1) operational statistics (utilization, departures, fleet size) from the HSCT operational analysis; (2) information such as fuel costs generated during the study; and (3) results of analysis of HSCT configurations, including block times, fuel burn, maintenance cost, and turnaround time. Figure 3-12 shows the percentage breakdown of cash operating cost for a current subsonic transport and the Mach 2.2 aircraft. Fuel, the predominant DOC item, has increased from about one-fourth of the cash operating cost for the subsonic aircraft to over one-third for the Mach 2.2 design. Ownership-related expenses are not included because the cash flow over the life of the HSCT is used to compute its value as an investment. Table 3-4 shows these costs for the Mach 3.2, 2.2, and Mach 1.6 configurations.

3.3.3 Operating Profit

Operating profit may be considered a measure of aircraft profitability. By deducting the operating cost from the revenues, operating profit can be calculated. Figure 3-13 shows the operating performance of the Mach 3.2, 2.2, and 1.6 configurations.

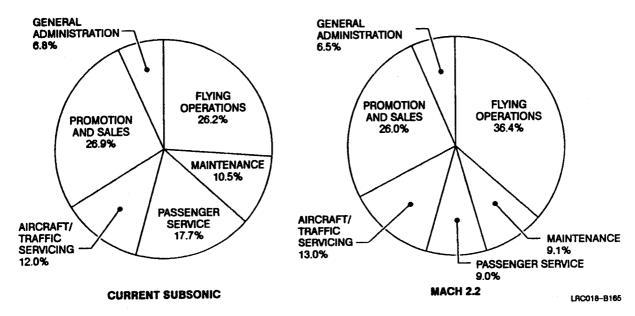


FIGURE 3-12. OPERATING COST BREAKDOWN - NO OWNERSHIP-RELATED COSTS

TABLE 3-4
OPERATING COST DATA FOR MACH 1.6, 2.2, 3.2 AIRCRAFT

		MACH 1.6	MACH 2.2	MACH 3.2
OPERATING COST PER SEAT-MILE	(\$)	0.05	0.048	0.047
OPERATING COST PER MILE	(\$)	15.51	14.36	14.18
OPERATING COST PER BLOCK HOUR	(\$)	14,414.00	16,769.00	21,711.00
OPERATING COST PER TRIP	(\$)	64,686.00	59,908.00	59,162.00
OPERATING COST PER AIRCRAFT PER YEAR	(\$)	44.9 MILLION	49.2 MILLION	59.2 MILLION

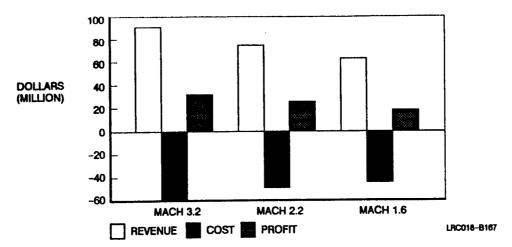


FIGURE 3-13. OPERATING PERFORMANCE (REVENUE - COST = PROFIT)

3.3.4 Aircraft Worth

Aircraft worth is the investment value of an airplane to the airline. The worth of an HSCT is estimated by an iterative process that determines the price to the operator so that a target rate of return on investment is achieved by the airline. Aircraft worth calculation includes corporate tax, depreciation, life of the asset, and the annual operating cash flow. Aircraft characteristics as well as operational parameters are embodied in the cash flow estimates. Results are shown in Tables 3-5 and 3-6 for various fare premiums and at a 10-percent return on investment to the airline.

3.3.5 Conclusion and Further Studies

Necessary conditions for economic viability include (1) airplane revenues covering operating costs plus an attractive rate of return to the operator, (2) fares compatible with subsonic fleet to expand HSCT service, and (3) a market large enough to permit a selling price lower than the investment value of the airplane. Market projections for the 2000 to 2025 time period indicate sufficient passenger traffic for ranges beyond 2,000 nautical miles to support a fleet of economically viable and environmentally compatible high-speed commercial transports. Fleet needs could total 2,300 or more 300-seat aircraft by 2025.

TABLE 3-5
ANNUAL CASH FLOW PER AIRCRAFT
(\$ MILLION)

FARE PREMIUM (PERCENT)	MACH 1.6	MACH 2.2	MACH 3.2
0	18.32	25.95	32.08
10	31.37	37.07	44.22
20	44.94	51.78	64.42
30	63.45	66.13	79.49
40	81.06	86.99	99.39
50	88.35	105.76	124.87

TABLE 3-6
AIRCRAFT WORTH AT 10-PERCENT ROI
(\$ MILLION)

FARE PREMIUM (PERCENT)	MACH 1.6	MACH 2.2	MACH 3.2
0	110	156	193
10	188	223	266
20	270	311	387
30	381	397	478
40	487	523	597
50	531	635	750

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Further analysis of the commercial value of the HSCT, comparing its economic worth to cost-based price, will be required. Additional assessments of HSCT economics will be made considering fuel prices, operational procedures, turnaround time, dispatch reliability, operating cost, and scenarios with and without the supersonic overland restriction. Parametric studies of different design ranges and passenger configurations will continue to be investigated in an effort to optimize the HSCT's economic viability.

SECTION 4 SUPERSONIC NETWORK EVALUATION

Future supersonic aircraft will bring major changes to long-range transportation. The new generation of aircraft will have to overcome many economic and environmental challenges before it can become a reality. The most constraining challenge is the global concern over the effect of engine emissions on the ozone layer, which protects life on earth from ultraviolet radiation. Community noise is another environmental challenge. The HSCT must meet at least the current subsonic noise certification standards to be compatible with the future subsonic fleet.

The sonic boom issue represents a major environmental and economic challenge as well. Supersonic operation overland produces the most desirable economic results. However, unacceptable overland sonic boom characteristics may force HSCT to use subsonic speeds overland.

Environmental concerns are likely to impose some restrictions on supersonic operation, thus introducing major changes to existing route structures and supersonic network composition. Concern over the atmospheric effect may restrict HSCT's cruise altitude and its proximity to the denser ozone layers. It may also interfere with great circle routes because of environmental impact on sensitive areas such as the North Pole. The current subsonic route structure may have to be altered to avoid sensitive areas in the stratosphere or to minimize overland flight tracks. It is important to examine the impact of these restrictions on the economic viability of the overall supersonic operation.

To be profitable, a supersonic transport must offer the traveling public significant time savings on long routes at acceptable fare premium levels. Under these assumptions, a potential market of about 2,000 aircraft will exist by the year 2025. This fleet size will enable engine and airframe manufacturers to build the plane at a cost that provides them with an attractive return on investment and to sell it at a price that allows the airlines to operate with a reasonable profit.

Subsonic overland operation of a supersonic aircraft hinders its economic viability for the following reasons:

- Reduced time savings
- Subsonic operation of a supersonic configuration imposes a penalty on its operating cost (e.g., increased fuel burn)
- Exclusion of some major city-pairs from the global supersonic network
- Increased airline dependence on fare premiums, thus reducing the HSCT's potential market share and profit

The effect of supersonic overland restriction on the aircraft's economic performance and the development of supersonic network scenarios will be investigated and discussed in this section.

4.1 AIRCRAFT ECONOMIC PERFORMANCE

4.1.1 Time Savings

Unrestricted supersonic operation produces optimum economic results. Time savings, the HSCT's most attractive marketing feature, would be maximized. As the percentage of subsonic overland increases, time savings decrease, thus eroding the unique competitive advantage of the HSCT over subsonic aircraft. Figure 4-1 shows how time savings decline at different levels of mixed operation. The highest time savings of supersonic versus subsonic flight is achieved for routes that are entirely overwater, such as between Honolulu and Sydney, where time savings exceed 5-1/2 hours. As the percentage of restricted operation increases, time savings decline, as for example the Dallas Fort Worth-Frankfurt route, where time savings are cut to 3 hours.

AVERAGE STAGE LENGTH - 4,500 NAUTICAL MILES SUBSONIC 10 **OFF-DESIGN** 9 **CRUISE SPEED MACH 0.95 BLOCK TIME MACH 1.6** (HOURS) 5 **MACH 3.2** 3 DFW-FRA SEA-SEL AKL-SIN 40 60 100

FIGURE 4-1. TIME PERFORMANCE

LRC018-B105

OVERLAND OFF-DESIGN OPERATION (PERCENT)

4.1.2 Operating Cost and Profit

There is a significant reduction in aircraft economic performance when a mixed mode of operation is gradually introduced. The impact of wholly supersonic versus mixed subsonic and supersonic flight on the vehicle's operating economics is illustrated in Figure 4-2. The data presented compare the operating revenue, cost, and profit for a vehicle with all Mach 2.2 operation versus vehicles with a mixed Mach number operation of Mach 2.2 overwater and 0.9 overland, or Mach 2.2 overwater and 1.6 overland. These comparisons are made with 10, 20, and 30 percent of the operation flown at the lower Mach number. At a 30:70 ratio of overland (Mach 1.6) to overwater (Mach 2.2) operation, there is an increase in operating cost of \$3 million annually per aircraft and \$1.3 billion for the global fleet. This reduces the vehicle's operating profit by the same amount. When the overland portion is flown at Mach 0.9, the increase in operating cost and the corresponding decrease in profit amounts to \$5 million per vehicle annually and \$2.2 billion for the global fleet.

(REVENUE - COST = PROFIT) MACH 2.2, MACH 2.2/1.6, MACH 2.2/0.9 (PER AIRCRAFT)

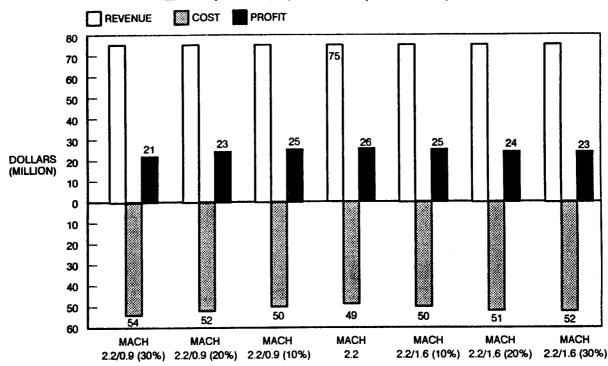


FIGURE 4-2. OPERATING PERFORMANCE

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A sonic boom-minimized aircraft at Mach 1.6 will economically outperform a vehicle with mixed operation of Mach 2.2 overwater and Mach 0.9 overland when the overland portion exceeds 30 percent of the flight. Figure 4-3 shows the percentage of cost to revenue and profit to revenue for Mach 2.2/1.6 and Mach 2.2/0.9 configurations at different percentages of subsonic operation. As the percentage of subsonic operation increases, the ratio of cost to revenue rises, while the ratio of profit to revenue declines: These ratios are compared to those of an all Mach 1.6 configuration. The unrestricted Mach 1.6 profitability ratio becomes higher than that of Mach 2.2/0.9 when the overland portion exceeds 28 percent, and higher than that of Mach 2.2/1.6 when the overland portion exceeds 50 percent.

The increase in operating cost is mostly due to the higher fuel burn of the mixed Mach number operation. Figure 4-4 illustrates the decline in HSCT miles per 1,000 pounds of fuel as the percentage of mixed operation increases over an average stage length of 4,500 nautical miles. For example, Mach 3.2 miles per 1,000 pounds of fuel burned declines by 13 percent when 20 percent of the operation is restricted to Mach 0.9 overland, and by 30 percent when the restricted overland portion reaches 60 percent of the flight.

4.1.3 Aircraft Worth

Aircraft worth, which is the investment value of an airplane to the airline operator, is also affected by restricted operation overland. An increase in the percentage of mixed Mach number operation reduces aircraft worth. Figure 4-5 shows that aircraft worth reaches its highest level at full supersonic operation. The data presented compare aircraft worth for vehicles with mixed Mach number operation versus an all Mach 1.6 sonic boom configuration

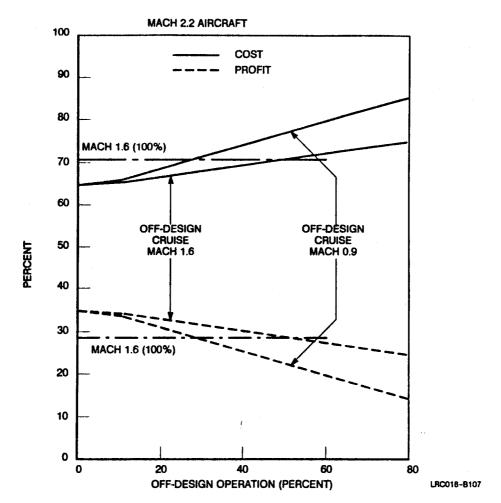


FIGURE 4-3. ECONOMIC PERFORMANCE PERCENTAGE OF OPERATING COST AND PROFIT TO REVENUE

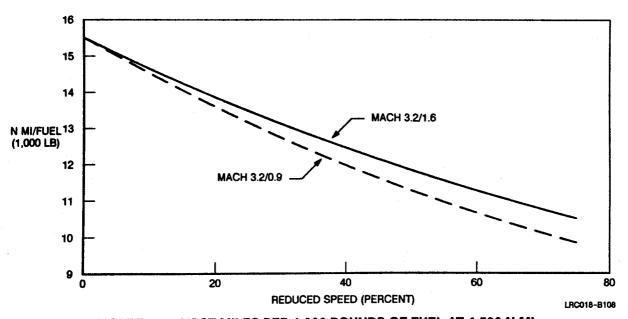


FIGURE 4-4. HSCT MILES PER 1,000 POUNDS OF FUEL AT 4,500 N MI

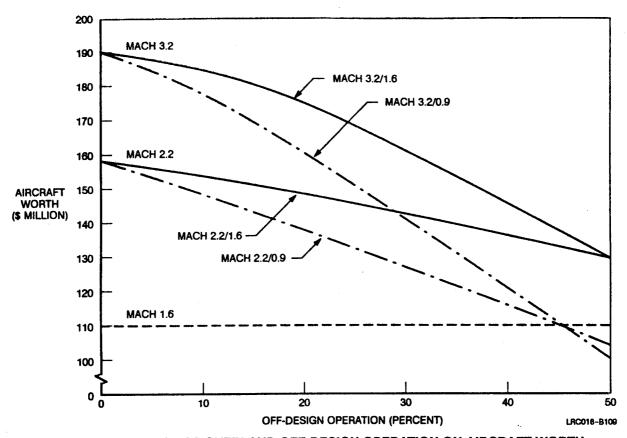


FIGURE 4-5. EFFECT OF OVERLAND OFF-DESIGN OPERATION ON AIRCRAFT WORTH

without performance penalties for refining the planform. Aircraft worth for both the Mach 3.2/0.9 and the Mach 2.2/0.9 continues to decline, intercepting the all Mach 1.6 worth at about 45 percent of restricted operation.

4.1.4 Fare Premium

Airlines can afford to charge the traveler a fare premium for the supersonic flight as long as the surcharge does not exceed the value of the time saved over a subsonic flight. Any restriction of supersonic operation overland will reduce time savings and thus affect the airlines' ability to charge a fare premium. Figure 4-6 explores the relationship between time savings and trip price, and identifies the break-even points of value of time saved and fare premium levels. The curves on the right side represent the value of time saved per class of travel. The left side shows where the value of time saved intercepts the value of fare premium per class. The figure also identifies the maximum level of fare premium the airlines may be able to charge per class of travel. To use this figure, simply locate the number of hours saved on the right side of the horizontal axis and move upward to the value of time saved per class. Move horizontally to the left and read the dollar value on the vertical axis. Continue horizontally across the chart toward the left side to intersect the value curve of the fare premium per class. Move downward to read the fare premium level on the left side of the horizontal axis. For example, the value of 6 hours of time saving for a first-class passenger is \$540. This value, when it intersects with the first-class fare premium curve, indicates the maximum level of fare premium the airlines may charge, which is 27 percent. The fewer the number of hours saved, the lower the level of fare premium the airline may be able to charge.

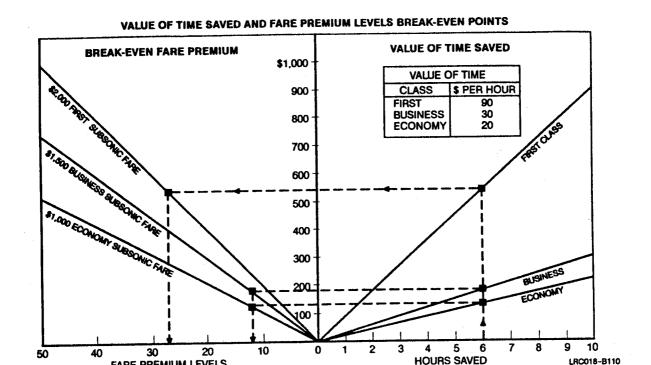


FIGURE 4-6. TIME SAVINGS AND TRIP PRICE RELATIONSHIP

In general, full supersonic operation is highly attractive to all concerned. It provides better economics for the airlines, the passengers, and the manufacturers. It is readily apparent that there are substantial economic and marketing benefits in full supersonic operation, and hence the importance of achieving a low-sonic-boom configuration.

SUPERSONIC NETWORK SCENARIOS

FARE PREMIUM LEVELS

Methodology 4.2.1

Supersonic restrictions overland and other environmental concerns may change some current subsonic global air route systems. MDC's route structure research group has been investigating several supersonic network scenarios, which were developed to assess the impact of environmental restrictions on the HSCT's market potential and economics. Attention is focused on reaching an optimum supersonic route structure to facilitate evaluation of different technical, operational, environmental, economic, and marketing scenarios that may ultimately influence the design of the HSCT. Figure 4-7 is a flowchart of supersonic network development. The process of structuring network scenarios starts with examining all international IATA regions and identifying the regions with the highest potential for supersonic operation.

The most current operational information on the world's airlines is reflected in their flight schedules as published in the Official Airline Guide (OAG). From the OAG on-line data base, all nonstop routes with a range greater than 2,000 statute miles were listed. Weekly departures, scheduled seats, aircraft miles, and seat miles were aggregated for each city-pair. The seat share for the city-pair was computed as a percent of the IATA region's total seats.

Information is reported for each IATA region by city-pairs sorted in descending order of scheduled seats. The long-range data extracted from the OAG world airline schedule include 900 city-pairs exceeding 2,000 statute miles. As shown in Figure 4-8, these city-pairs are

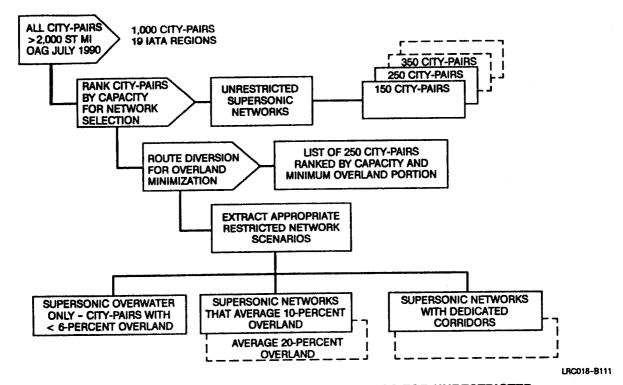
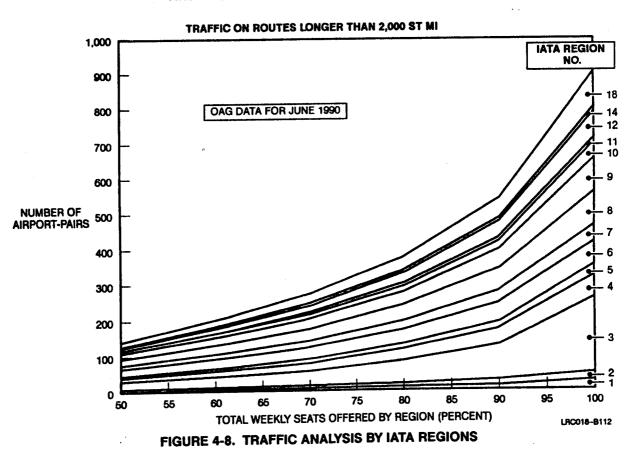


FIGURE 4-7. SUPERSONIC NETWORK SCENARIOS FOR UNRESTRICTED AND RESTRICTED OPERATION



distributed among 14 IATA regions. Not all of these city-pairs are necessarily candidates for HSCT service. The most logical candidates are the high-density traffic routes, defined by scheduled seat capacity.

Using the long-range data set, sorted in descending order of scheduled seats, many subsets of top city-pairs can be selected as unrestricted supersonic network scenarios. These supersonic network scenarios can only be used if a low-boom configuration is successfully developed. To visualize the global network formed by the top 250 city-pairs, their great circle routes were plotted on a world map in Figure 4-9.

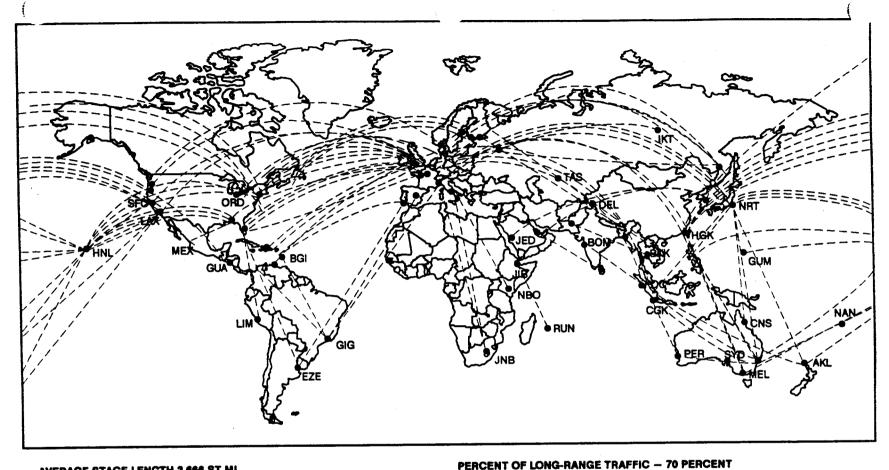
4.2.2 Route Diversion Analysis

Until a satisfactory solution to the sonic boom problem is obtained, supersonic flight overland will be restricted. Modifications to great circle routes are required to find an alternative flight path that eliminates or minimizes overland flight to unpopulated land masses. Using the long-range data set, a subset of the top 250 city-pairs was selected to conduct route diversion analyses. The basic traffic data for the 250 city-pairs are presented in Appendix A. The traffic data are also sorted by departures, aircraft miles, annual seat miles, and aircraft hours. This ranking highlights the fact that membership in the top set is controlled by the choice of ranking criteria.

The 250 candidate city-pairs route were each analyzed for possible diversion to eliminate or reduce overland tracks. The process involved generating a strip chart for each candidate route. A strip chart is an oblique map projection showing an area 15 to 20 degrees on either side of the great circle track between origin and destination. By selecting the great circle route to be the equator of the projection, the highest possible scale accuracy is obtained for the chart. From such charts, diverted routes can be designed, and overland segments, if any, can be measured directly. Figure 4-10 shows the strip chart for the London-New York route. Data presented in Figure 4-10 show that the overland track has been reduced more than 20 percent through diversion, while the increase in great circle distance is limited to only 3 percent. The generated strip charts of a few key routes are presented in Appendix B.

The results of the route diversion analysis are summarized in Appendix C. The table compares the overland portions of the diverted route and its original great circle route. Some of the routes are all overwater with no diversion required. Others become all overwater through diversion. Still others exhibit various degrees of overland reduction through diversion. However, some are all overland, where no feasible diversion is possible. The all-overland routes are strong candidates for removal from possible HSCT service.

In evaluating flight performance, the ground track profile becomes important. If the overland segments of the route occur at the beginning and end of the flight, performance is least affected. However, if the overland segments happen to fall anywhere along the track after cruise speed has been reached, performance penalties can be severe. The aircraft must fly lower and slower over the land segment and then climb back up to higher cruise altitude. The amount of fuel burned by this maneuver depends on how heavy the aircraft is at the start of the maneuver. The ground track profiles on a normalized linear scale are summarized in Appendix C. Each track profile is flagged according to the type it exhibits. Type 1 profile is all overwater or has overland portions at either end of the track. Type 2 is a profile with over-



AVERAGE STAGE LENGTH 3,666 ST MI

- 1. NORTH AMERICA SOUTH AMERICA (5) GIG-MIA NO. 20
- 2. NORTH AMERICA CENTRAL AMERICA (6) JFK-MEX NO. 61
- 3. NORTH TRANSATLANTIC (69) JFK-LHR NO. 2
- 4. MID TRANSATLANTIC (10) MAD-MIA NO. 132
- 5. SOUTH TRANSATLANTIC (3) GIG-MAD NO. 120

- 7. EUROPE SOUTH AFRICA (3) JNB-LHR NO. 101
- 8. EUROPE MIDDLE EAST (12) **DXB-LON NO. 78**
- 9. EUROPE FAR EAST (26) NRT-SVO NO. 24
- 10. AMERICAS MID PACIFIC (23) HNL-NRT NO. 10
- 11. AMERICAS SOUTH PACIFIC (5) AKL-HNL NO. 50

- 12. WITHIN NORTH AMERICA (55) HNL-LAX NO. 1
- 16. WITHIN AFRICA (1) JIB-RUN NO. 245
- 18. WITHIN FAR EAST (25) NRT-SIN NO. 12
- 19. MISCELLANEOUS (8) BKK-DXB NO. 84

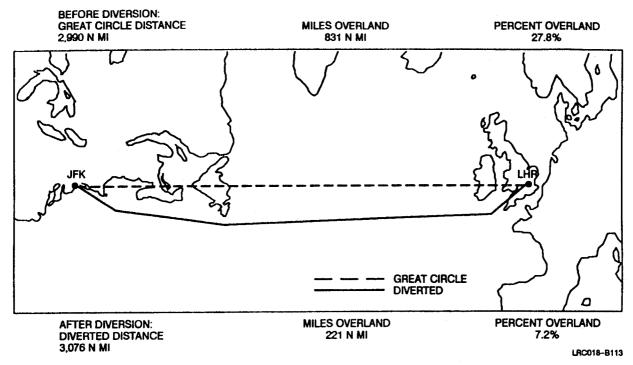
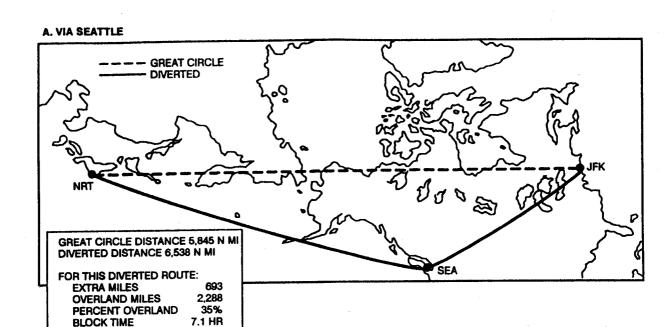


FIGURE 4-10. CITY-PAIR EVALUATION - JFK (NEW YORK)-LHR (LONDON)

land segments anywhere in the middle of the track. Type 3 consists of tracks exhibiting more than 50 percent of overland segments, which are candidates for elimination. Type 4 identifies tracks that are 100-percent overland. An example of route diversion and optimization is depicted in Figure 4-11 for the New York-Tokyo route. By rerouting the flight via Seattle, distance increased by 693 miles, and the percentage overland declined from 88 to 35 percent, as illustrated in Figure 4-11A. By diverting the route through the Arctic Ocean, Bering Strait, and North Pacific, the percentage of overland flight was further reduced to 20 percent at a cost of 227 extra nautical miles, as shown in Figure 4-11B. The ground track profile is displayed on a normalized scale in Table 4-1.

The 250-network scenario represents 64 percent of the annual seat-miles for long-range routes over 2,000 statute miles. The average impact of route diversion compared to the great circle route is a 4-percent increase in network distance and a 41-percent reduction in overland distance. To visualize the global network formed by the top 250 city-pairs, their great circle routes were plotted on a world map in Figure 4-12. A 150 city-pair network is also considered as a candidate supersonic scenario. The 150-network scenario is similar to the 250 city-pair scenario without the bottom 100 city-pairs. The 150-network scenario represented 52 percent of the annual seat-miles for all long-range routes over 2,000 statute miles. Although the 150 city-pair network is structurally only 60 percent of the 250 city-pair network, 80 percent of the traffic is still present. The average impact of route diversion compared to the great circle routes is a 5-percent increase in network distance and a 41-percent reduction in overland distance. The great circle routes for the 150 city-pair network are shown in Figure 4-13. The most apparent feature, when the map is compared to the 250-network map, is that the global pattern does not change, but gets denser.





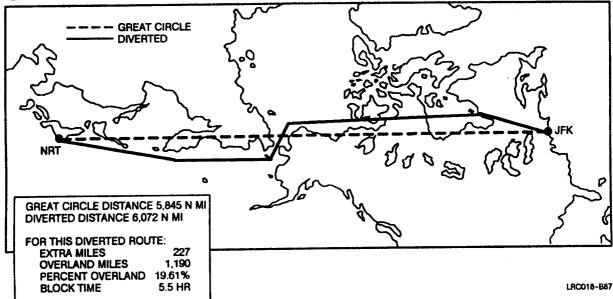


FIGURE 4-11. DIVERTED ROUTING - NEW YORK-TOKYO

4.2.3 Overwater Network Scenario

The basic HSCT 250-network scenario was based on the high-density traffic as reported by the OAG. The ground track display shows a mix of desirable and undesirable flight profiles, and some routes that exhibit a high percentage of overland portions. The 250 city-pairs list sorted in descending order of scheduled seats in Appendix A was resorted in ascending order of percentage of the overland segment, as shown in Appendix C. All routes exhibiting more than half the distance overland were eliminated. A list of 207 city-pairs, with an overland portion that does not exceed half the distance in each case, was used to extract a variety of supersonic network scenarios. For example, to extract an all-overwater network, only routes with a 6-percent overland segment, 3 percent for climb and 3 percent for descent, would be

TABLE 4-1.
EXAMPLE OF GROUND TRACK PROFILE DISPLAY FOR NEW YORK-TOKYO

	00								GROU	ND TF	RACK I	LENG	TH (%)			
AIRPORT PAIR	GC RANGE (N MI)	DIVERTED RANGE	DIST	OVERLAND (%)	FLAG	0	1 0	2	3 0	4	5 0	6	7	8	9	
LIM-MIA	2,277	2,647	183	6.9	2	1			111							
CPH-SEA	4,214	5,074	624	12.3	2	11							111	11		
LHR-NRT	5,147	5,880	759	12.9	2	1							11111			
EZE-MIA	3,831	4,137	691	16.7	2	111	1111	İ						1		
FRA-NRT	5,063	5,211	917	17.6	2	ı						1		11		
> JFK-NRT	5,845	6,072	1,190	19.6	2	111			1111							
CDG-NRT	5,237	5,607	1,110	19.8	2	1			_			111111			
LAX-LHR	4,727	5,138	1,978	38.5	2				11111		111		111		- 1	11,
LAX-LGW	4,747	5,138	1,978	38.5	2				111111	-	111		111		- 1	111
BKK-DXB	2,635	2,635	1,415	53.7	2	111	1111			1111	11111	11 11	1111			
MEL-SIN	3,260	3,260	1,757	53.9	3				11111					I		
BKK-KHI	1,998	1,998	1,451	72.6	3										11 11 1	111
LHR-SIN	5,872		4,886	83.2	3				88888						111	
NRT-SVO	4.048	4,048	3,663	90.5	3	Ш		1111	111111	11111	11111	11111	111111		16 68 8 8	111
BKK-FCO	4,775	4,775	4,775	100.0	4	111			111111		11111			4 I I I I	11111	111

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selected. Under these assumptions, only 100 city-pairs would qualify for the overwater network scenario. Figure 4-14 shows the great circle routes of the 100 city-pair overwater network. The 100 overwater network represents 28 percent of total long-range annual seatmiles. The average impact of route diversion compared to the great circle route is a 6-percent increase in network distance and a 92-percent reduction in overland distance.

To structure a network with an overland portion averaging 10 percent of the total network, the top 200 city-pairs are selected from the same list. The 200 network carries 50 percent of long-range annual seat-miles. It covers 13 IATA regions and has an average stage length of 3,998 statute miles. An increase of 5.7 percent in distance results in a 69-percent reduction in overland segments. Figure 4-15 illustrates the great circle route structure of the 200 city-pairs on the world map.

4.3 CONCLUSION

Only a few candidate global airline network scenarios for HSCT have been assembled. They are patterned after the high-density long-range markets from the OAG on-line data base. Creative rerouting was conducted to minimize overland segments and to lessen the impact of the environmental restrictions that may be imposed on future supersonic operation.

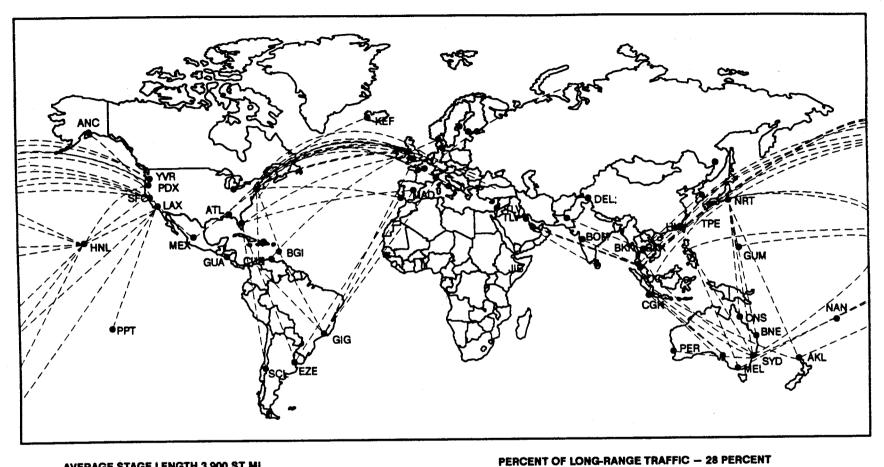
The data on these network scenarios represent an assembly of global routes from which HSCT global traffic networks can be constructed. The network scenarios provide examples on how supersonic service may bring some changes to the current global route structure. Some of these supersonic network scenarios show good potential of capturing more than half the market share of the long-range traffic.

4.4 RECOMMENDATIONS FOR FURTHER STUDY

Further analysis is still required to accurately assess the effect of these supersonic network scenarios on aircraft economic performance, productivity, and fleet projections. Supersonic network research and development will continue to search for more ways to respond to the environmental concerns, operational policies, marketing strategies, and specific network requirements of customer airlines.

FIGURE 4-12. HSCT TOP SEAT RANK 250 AIRPORT-PAIRS

FIGURE 4-13. HSCT TOP SEAT RANK 150 AIRPORT-PAIRS



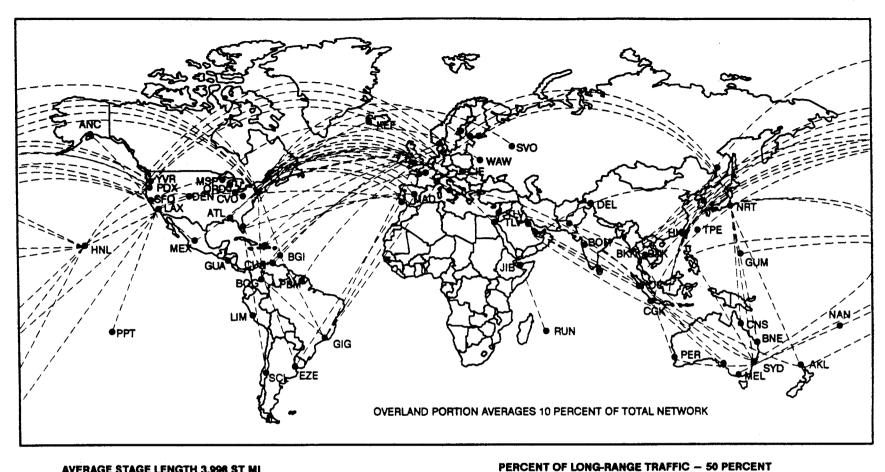
AVERAGE STAGE LENGTH 3,900 ST MI

- 1. NORTH AMERICA SOUTH AMERICA (4) GIG-JFK NO. 16
- 2. NORTH AMERICA CENTRAL AMERICA (3) BGI-JFK NO. 19
- 3. NORTH TRANSATLANTIC (26) JFK-CDG NO. 80
- 4. MID TRANSATLANTIC (5) MAD-MIA NO. 99

- 5. SOUTH TRANSATLANTIC (5) GIG-MAD NO. 87
- 10. AMERICAS MID PACIFIC (19) HNL-NRT NO. 2
- 11. AMERICAS SOUTH PACIFIC (6) AKL-HNL NO. 10
- 12. WITHIN NORTH AMERICA (8) HNL-LAX NO. 1

- 18. WITHIN FAR EAST (20) NRT-SIN NO. 6
- 19. MISCELLANEOUS (4) DXB-KUL NO. 68

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AVERAGE STAGE LENGTH 3,996 ST MI

- 1. NORTH AMERICA SOUTH AMERICA (7) GIG-MIA NO. 69
- 2. NORTH AMERICA CENTRAL AMERICA (6) JFK-MEX NO. 89
- 3. NORTH TRANSATLANTIC (83) JFK-LHR NO. 112
- MID TRANSATLANTIC (14) MAD-MIA NO. 99
- 5. SOUTH TRANSATLANTIC (5) GIG-MAD NO. 87

- 8. EUROPE MIDDLE EAST (5) LHR-TLV NO. 180
- 9. EUROPE FAR EAST (5) LHR-NRT NO. 142
- 10. AMERICAS MID PACIFIC (28) HNL-NRT NO. 2
- 11. AMERICAS SOUTH PACIFIC (6) AKL-HNL NO. 26
- 12. WITHIN NORTH AMERICA (14) HNL-LAX

- 16. WITHIN AFRICA (1) JIB-RUN NO. 177
- 18. WITHIN FAR EAST (22) NRT-SIN NO. 6
- 19. MISCELLANEOUS (4) DXB-KUL NO. 68

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SECTION 5 ATMOSPHERIC EMISSIONS IMPACT STATUS

Atmospheric emissions impact studies focused on generating inputs for two-dimensional global atmospheric chemistry models. Airframe concepts at Mach 1.6, Mach 2.2, and Mach 3.2 were used in conjunction with several low-NO_x candidate engine concepts from both Pratt & Whitney and General Electric. The procedure used to generate the atmospheric model inputs was upgraded and automated under independent research funds. A brief description of the procedure is included in this report and a complete description of the new methodology is provided in NASA CR 181882.

The impact of atmospheric emissions for airframe/engine concepts on global ozone concentrations was estimated through correlation with Lawrence Livermore National Laboratories (LLNL) two-dimensional (2-D) atmospheric model runs. A large matrix of emission scenarios was provided to LLNL by Douglas under an independent research effort, and estimates of global ozone impact were generated with the LLNL two-dimensional global atmospheric model. The emissions scenarios developed for the 1990 emission studies were cross-referenced with the independent research results to arrive at an estimated global ozone column change. These estimates are included in this report.

The potential impact of regulations restricting cruise altitude was investigated in terms of economic penalties and ozone benefits. Baseline aircraft at Mach 1.6, 2.2, and 3.2 were flown with several different cruise altitude ceiling limits. Fuel burn and emission constituent data were generated for these restricted flight paths and compared to baseline cases. The ozone impact of these restrictions was then estimated by cross-referencing the results with the LLNL 2-D model runs described above. Economic impact in terms of operating cost and aircraft worth were quantified. These studies provide insight into the feasibility and practicality of protecting atmospheric ozone through cruise altitude restrictions.

5.1 BRIEF METHODOLOGY REVIEW

The operational network of an HSCT is broken down into 10 IATA regions worldwide. For each of these regions, a city-pair is chosen that best describes the average latitude distribution. The 10 regions, along with their corresponding city-pairs, are shown in Figure 5-1. A mission is flown for each city-pair with the airframe/engine combination in question to determine the fuel burn in each region as a function of altitude and latitude. The 10 regions are then compiled into one data set representing the total annual worldwide fuel burn in each latitude and altitude band as specified by the 2-D atmospheric models.

Final input to the global atmospheric models is broken down into seven distinct engine emission constituents. These are NO, NO₂, SO₂, CO, H₂O, CO₂, and THC (trace hydrocarbons). In addition, summary data for all oxides of nitrogen are provided (NO+NO₂) as NO_x. The total constituent emissions are determined by multiplying the total fuel burn by the emission index for each constituent.

The worldwide fuel burns are a function of many parameters, including economic forecasts for the time period in question. An overall data flowchart is presented in Figure 5-2. This chart shows the dependency of the emissions data on a wide array of estimates and

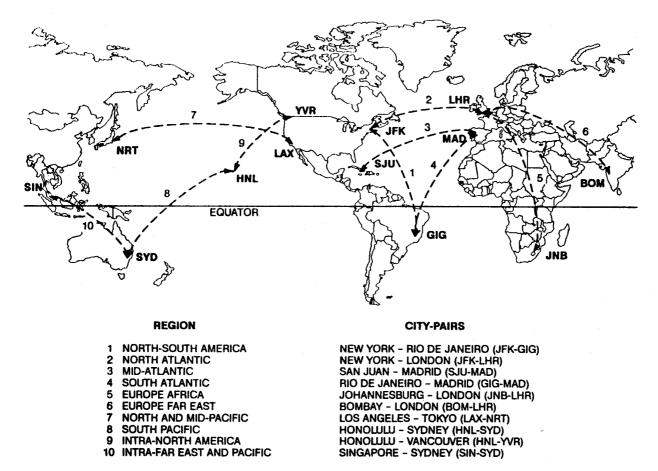


FIGURE 5-1. HSCT REPRESENTATIVE CITY-PAIRS

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assumptions concerning not only aircraft and engine performance, but also passenger demand forecasts.

5.2 ATMOSPHERIC EMISSION SCENARIOS

Emissions forecasts were developed for five engines — a P&W Mach 1.6 turbine-bypass engine (TBE), P&W Mach 2.2 TBE, P&W Mach 3.2 TBE, P&W Mach 3.2 variable-stream-control engine (VSCE), and GE Mach 3.2 variable-cycle engine (VCE). All five combustors contained a low-NO_x combustor design in the 5-EINO_x range. Douglas baseline missions were flown for each of the airframe/engine combinations. The airframes used at each Mach number correspond to the baseline configurations described earlier. Mission profiles were all supersonic with no allowance for subsonic overland operations. Table 5-1 shows the total annual fuel burn by region for each engine as determined through a complete performance analysis.

Complete input data sets for 2-D global atmospheric chemistry models were created for each engine concept. These data sets are very large and are not included in this report. The complete data sets for the P&W TBE engines can be found in NASA CR 181882. These data sets were generated by breaking the total mission into four segments — takeoff, climb, cruise, and descent. Emission indices were determined at each of the four segments on the basis of

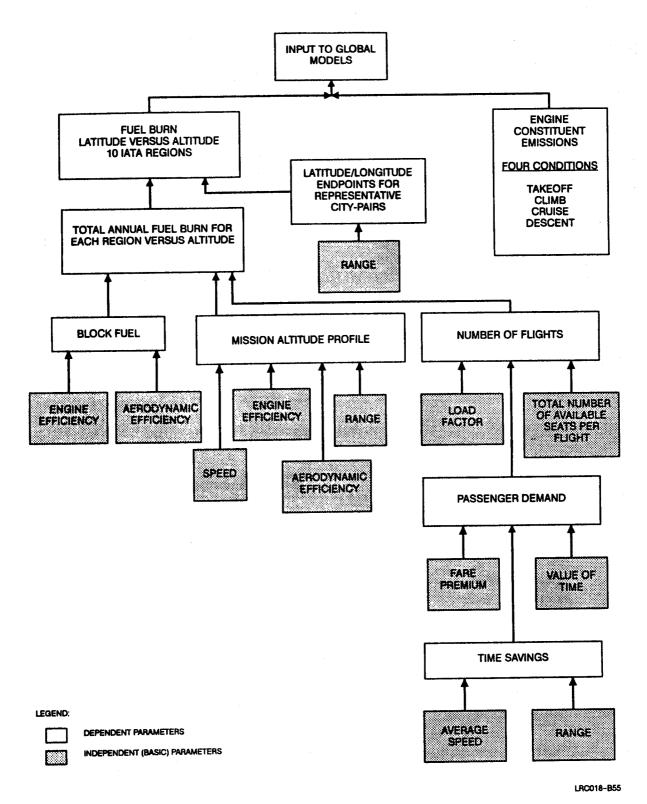


FIGURE 5-2. DATA FLOW FOR GENERATING INPUTS TO GLOBAL ATMOSPHERIC MODELS

data supplied by the engine manufacturers. This is believed to improve the fidelity of the emissions estimates compared to methods that consider only the cruise segment. NO_x emission indices for each engine concept at the various operating conditions are presented in Table 5-2.

TABLE 5-1
TOTAL ANNUAL FUEL BURN BY REGION

			FUEL BURN (10	LB)	
REGION	P&W MACH 1.6 TBE	P&W MACH 2.2 TBE	P&W MACH 3.2 TBE	P&W MACH 3.2 VSCE	GE MACH 3.2 VCE
NORTH-SOUTH AMERICA	1,729	1,735	1,864	2,371	2,133
NORTH ATLANTIC	20,029	20,168	21,774	27,656	24,889
MID-ATLANTIC	1,445	1,453	1,565	1,985	1,788
SOUTH ATLANTIC	2,262	2,255	2,393	3,039	2,730
EUROPE-AFRICA	4,339	4,391	4,791	6,110	5,493
EUROPE-FAR EAST	6,805	6,814	7,283	9,224	8,296
NORTH AND MID-PACIFIC	23,992	23,934	25,411	32,261	28,968
SOUTH PACIFIC	2,612	2,618	2,806	3,563	3,202
INTRA-NORTH AMERICA	159	163	182	231	209
INTRA-FAR EAST AND PACIFIC	10,390	10,527	11,487	14,594	13,133

TABLE 5-2
NO_X EMISSION INDICES FOR VARIOUS ENGINE CONCEPTS

		EI = LB/1,000 L	B FUEL BURNED	
ENGINE	TAKEOFF EI	CLIMB EI	CRUISE El	DESCENT EI
P&W MACH 1.6 TBE	5.5	6.7	5.3	3.7
P&W MACH 2.2 TBE	3.5	6.1	4.5	2.7
P&W MACH 3.2 TBE	3.5	7.9	5.1	1.5
P&W MACH 3.2 VSCE	2.3	4.5	4.4	4.5
GE MACH 3.2 VCE	3.6	7.8	6.3	10.1

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5.3 OZONE IMPACT TRADE STUDIES

The baseline emissions scenarios developed for this task were used in conducting trade studies to investigate the effects of parameters such as fleet size, fare premium, Mach number, year of service, and engine type on the global ozone concentration as predicted by the LLNL 2-D model (through correlation with IRAD data).

The cruise Mach number of an aircraft determines its optimum cruise altitude and has a strong impact on the fuel burn. Higher Mach numbers lead to higher cruise altitudes and typically result in increased fuel consumption. Researchers have shown that the impact of aircraft emissions on ozone is very sensitive to injection altitude, particularly in the stratosphere at about 70,000-80,000 feet. As this altitude is approached by increasing Mach number, the impact of the NO_x emissions increases. This effect is shown in Figure 5-3 by the baseline

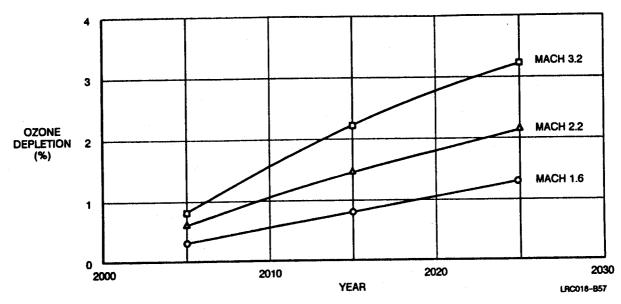


FIGURE 5-3. OZONE DEPLETION BY YEAR - P&W TBE ENGINE

emissions scenarios. From this plot, it is readily seen that column ozone depletion is a strong function of Mach number. The figure also shows that ozone concentration is further decreased as the fleet size is increased over a period of production years. In the 20 years from 2005 to 2025, the ozone impact of HSCT emissions based on passenger demand may be expected to increase by a factor of four.

The difference in ozone depletion between the three engine types is shown in Figure 5-4. This figure illustrates the problem of relying solely on EINO_x as the figure of merit for ozone depletion. The P&W VSCE has the lowest EINO_x value of all the Mach 3.2 engines, as indicated in Table 5-2, but the mission fuel burn was higher than that for the P&W TBE. This resulted in a larger impact on global ozone concentration for the VSCE. This emphasizes the

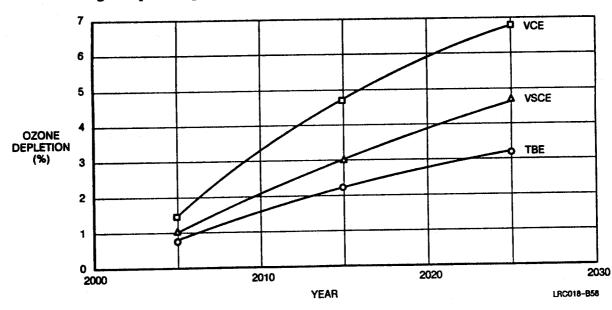


FIGURE 5-4. OZONE DEPLETION VERSUS ENGINE TYPE - MACH 3.2

need for the engine manufacturers to maintain high cruise efficiency while improving EINO_x combustor standards.

A direct comparison of fleet size, number of flights, and ozone depletion is shown in Figure 5-5. The ozone depletion for a given fleet size is found by cross-referencing the fleet size with the number of flights for the appropriate Mach number. The number of flights can then be translated vertically to the top plot to determine the column ozone depletion. For a given annual passenger demand, and hence number of flights, the ozone impact is greater for a Mach 3.2 fleet than for a Mach 1.6 fleet, even though the Mach 3.2 fleet is smaller.

Logically, it would be assumed that a larger fleet size would lead to a greater ozone impact. This is not always the case, however, because the important parameter is actually the number of flights. One aircraft making 1000 annual flights will have a greater ozone impact than 500 aircraft making one annual flight. This effect is important when comparisons are made for different Mach numbers. Faster airplanes can make more flights per day, thereby allowing for smaller fleet sizes to achieve equal productivity. Therefore, the Mach 3.2 fleet is smaller

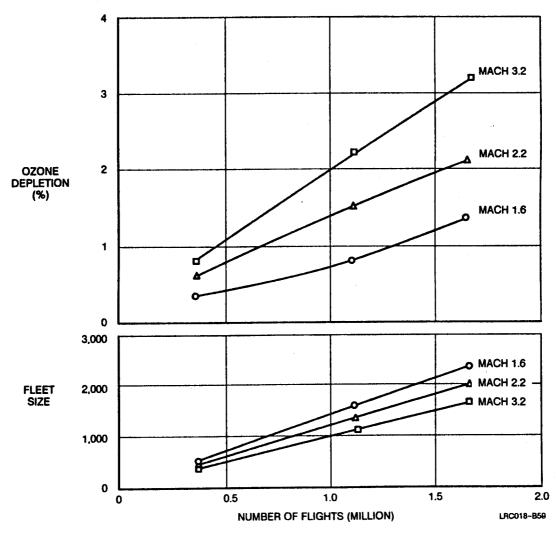


FIGURE 5-5. OZONE DEPLETION AND FLEET SIZE VERSUS NUMBER OF FLIGHTS FOR P&W TBE

than the Mach 2.2 or Mach 1.6 fleet for an equivalent number of annual flights and equal productivity.

One important economic parameter to consider is fare premium, i.e., the percentage increase of an HSCT fare over an equivalent subsonic fare. Current baseline design objectives include zero fare premium. This is considered to be optimistic with regard to the operating cost of an HSCT, but conservative with regard to ozone impact. Optimistic lower fare premiums create higher passenger demands, and hence, more flights. This relationship was shown earlier in Figure 5-2. A plot showing the impact of fare premium for Mach 3.2 and Mach 1.6 scenarios is shown in Figure 5-6. This figure compares a baseline 0-percent fare premium

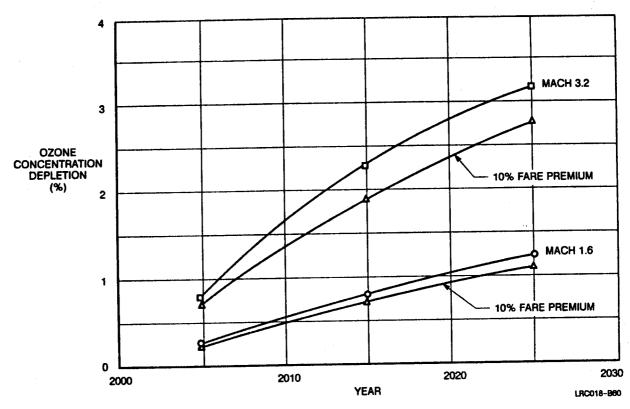


FIGURE 5-6. FARE PREMIUM IMPACT ON OZONE CONCENTRATION

with a 10-percent fare premium. As can be seen, an increase in fare premium reduces ozone impact by reducing the number of annual flights.

The 1990 emissions trade studies show that there is a wide range in the potential ozone impact from HSCT aircraft depending on the economic and flight performance of the fleet. These studies highlight approaches for minimizing ozone impact as well as approaches that should be avoided. The sensitivity of the results to tentative economic assumptions also reveals the uncertainty involved in the evaluation of emissions impact for a fleet of HSCTs.

5.4 CRUISE ALTITUDE RESTRICTIONS

One potential means of regulating and controlling the impact of supersonic aircraft emissions on atmospheric ozone is for international regulators to mandate a cruise altitude ceiling for

supersonic flight, ensuring that NO_x is not emitted in the more sensitive altitude bands. The economic and performance impacts of such a regulation are strongly influenced by Mach number, optimum cruise altitude of the aircraft, and the cruise restriction altitude. For instance, a 60,000-foot ceiling restriction is not likely to have any impact on a Mach 1.6 configuration, but would significantly erode the performance of a Mach 3.2 configuration and, to a lesser extent, that of the Mach 2.2 configuration.

A series of cruise altitude restrictions were applied to the three baseline configurations to investigate the overall economic and ozone concentration impacts. Altitude restrictions ranging from 40,000 to 80,000 feet were applied to the Mach 1.6, 2.2, and 3.2 aircraft. The impact of these restrictions on ozone concentration is shown in Figure 5-7. Altitude restrictions at

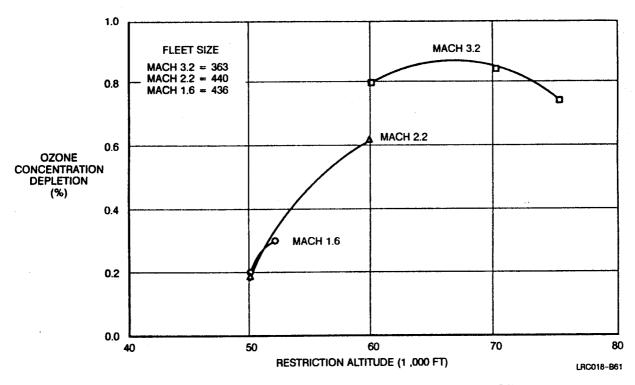


FIGURE 5-7. CRUISE ALTITUDE RESTRICTION OZONE IMPACT

Mach 3.2 tended to actually increase the ozone impact because of the sharp increase in fuel burn resulting from off-design operation. Altitude restrictions at 50,000 feet and below had a favorable ozone impact on the Mach 2.2 and Mach 1.6 aircraft, driving the estimated ozone depletion down to less than 0.5 percent. In general, the effectiveness of the restrictions is increased as the ceiling altitude is lowered.

As would be expected, HSCT economic performance deteriorates when the vehicle is operated away from its optimum design altitude as a result of higher fuel consumption, reduction in the aircraft design range, and a loss of some long-range routes. Resizing the aircraft is a means to regain lost range, but will result in a weight and performance penalty proportional to the amount of range that must be recovered. Figure 5-8 shows the relationship between weight and range penalties for cruise altitude restrictions at Mach 3.2. The left side of the

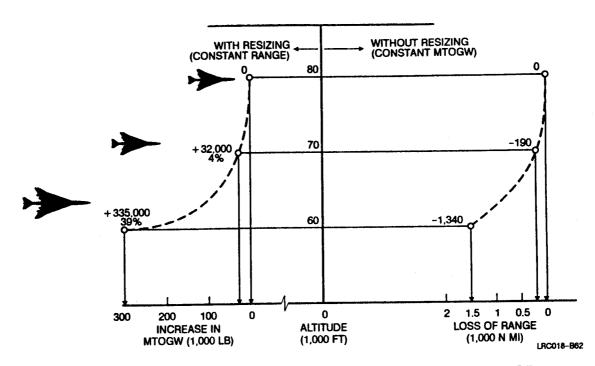


FIGURE 5-8. EFFECTS OF CRUISE ALTITUDE RESTRICTION ON MTOGW AND RANGE - MACH 3.2

chart describes the weight impact of resizing the vehicle, while the right side describes the range penalty incurred without resizing.

While resizing the aircraft is a viable means of regaining lost range, it is probably not practical for an HSCT in light of the significant weight and performance penalties associated with it. In most cases, the Mach number of an aircraft would be lowered before it would be resized to fly at off-design altitudes. The one scenario that would require resizing at off-design altitudes would be the imposition of cruise altitude restrictions well into the development phase when the engine and airframe are beyond a point of no return. For this reason, the following economic analysis of cruise altitude restrictions is focused on baseline vehicles with no resizing. The effect of cruise altitude restrictions on the operating economics will be examined for the following scenarios as indicated in the matrix below.

CRUISE ALTITUDE	MACH 3.2	MACH 2.2	MACH 1.6
80,000 FT	X		
70,000 FT	x	X	
60,000 FT	x	X	X
50,000 FT		X	X
40,000 FT			X

Cruise altitude restrictions will affect the economics of an HSCT in several ways. One prominent effect will be a reduction in market capture caused by the loss of long-haul routes (citypairs) as a result of the range penalty. This effect is shown for the Mach 3.2 vehicle in terms of annual seat-miles (ASMs) in Figure 5-9. A 60,000-foot restriction, for instance, is estimated to reduce ASMs by 14 percent.

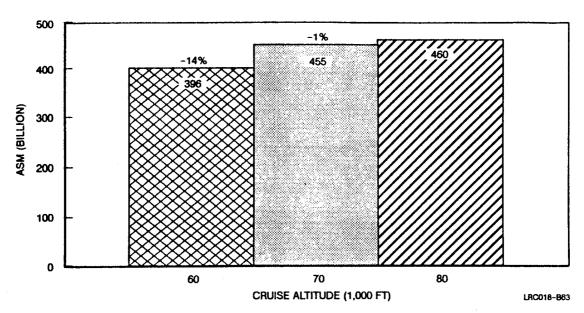


FIGURE 5-9. EFFECT OF CRUISE ALTITUDE RESTRICTION ON MARKET CAPTURE (ANNUAL SEAT-MILES)

Cruise altitude restrictions will increase HSCT operating cost and will subsequently reduce operating profit. This effect is increased as the altitude restrictions become more severe, as illustrated in Figure 5-10 for a Mach 3. 2 vehicle. The breakdown of operating cost for three cruise altitude restriction scenarios is shown in Figure 5-11. These pie graphs show how the fuel cost is driven up while profits go down for increasingly severe restrictions. The strong dependency of operating cost on fuel for these altitude restrictions is shown in Figure 5-12.

Aircraft worth, a parameter that estimates the investment value of an aircraft to an airline operator, also declines when aircraft are restricted to off-design cruise altitudes. The decline in aircraft worth and operating profit for a Mach 3.2 vehicle at restricted cruise altitudes is

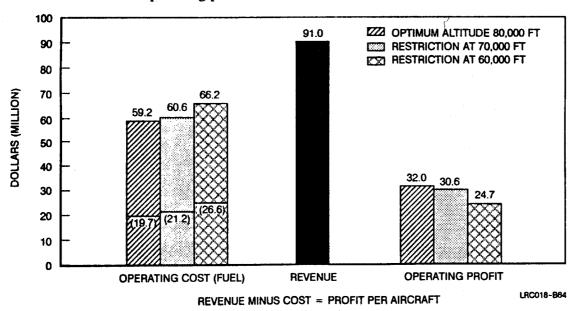
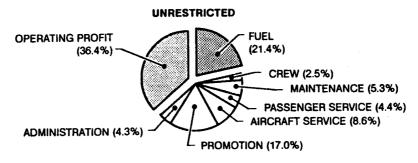


FIGURE 5-10. EFFECT OF CRUISE ALTITUDE ON OPERATING PERFORMANCE - MACH 3.2



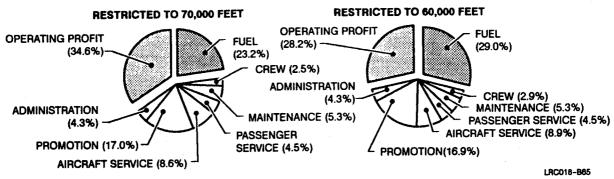


FIGURE 5-11. EFFECT OF CRUISE ALTITUDE RESTRICTIONS ON OPERATING COST AND PROFIT - MACH 3.2

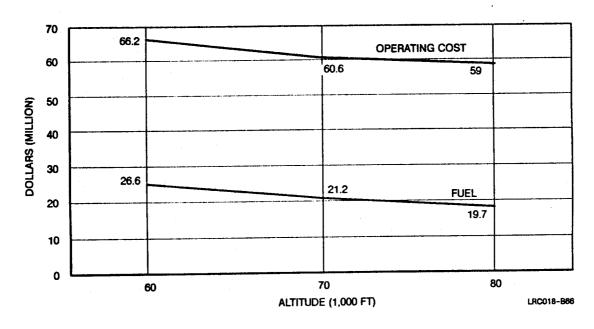


FIGURE 5-12. EFFECT OF CRUISE ALTITUDE RESTRICTION ON OPERATING COST AND FUEL COST - MACH 3.2 WITHOUT RESIZING

illustrated in Figure 5-13. At 70,000 feet the aircraft worth declined by 4 percent, and at 60,000 feet the aircraft worth showed a stronger decline of 23 percent. The close relationship between profit and aircraft worth is reflected by the equivalent rate of decline for these parameters at off-design cruise altitudes.

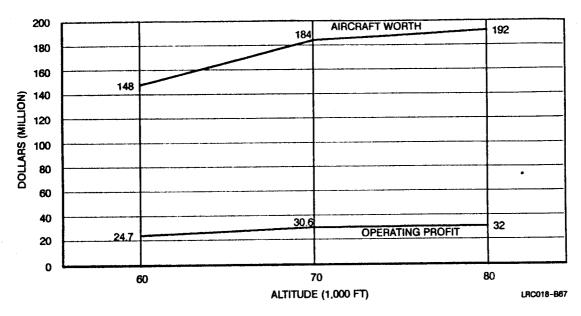


FIGURE 5-13. EFFECT OF CRUISE ALTITUDE ON AIRCRAFT WORTH AND OPERATING PROFIT – MACH 3.2 WITHOUT RESIZING

A summary of the economic impact of cruise altitude restrictions is provided in Table 5-3. Shown are the operating cost, profit, and aircraft worth, with corresponding percentage changes. Portions of these data are displayed graphically in Figure 5-14. This figure shows that the expected increase in aircraft worth with increasing Mach number at a design range of 6,500 nautical miles can be counteracted by altitude restrictions. For instance, the Mach 2.2 operating profit and aircraft worth exceeds that of the Mach 3.2 aircraft for a 60,000-foot restriction.

5.5 CONCLUSIONS

- Results showed that ozone depletion is a function of the cruise Mach number of the aircraft, primarily because of the strong dependence of ozone impact on injection altitude.
- For the P&W turbine bypass engine with a cruise EINO_x of approximately 5, the only configuration that results in ozone depletions in the 1-percent range is the Mach 1.6

TABLE 5-3
AIRCRAFT ECONOMIC PERFORMANCE AT DIFFERENT CRUISE ALTITUDES

CRUISE			IG CC						FIT (\$ ENT O		ION) ANGE		AIRC	RAF PERC	T WOF	TH (MILI	JON)
ALTITUDE (1,000 FT)	M3.2	%	M2.2	%	M1.6	%	M3.2	%	M2.2	%	M1.6	%	M3.2	%	M2.2	%	M1.6	%
80	59	·					32						192					
70	60.6	+2.7	49				30.6	-4.4	26				184	-4	156			
60	66.2	+ 12	50	+2	45		24.7	-23	25	-4	18		148	-23	151	-3	110	
50			54	+ 10	46	+2			20	-23	17	-6			125	-20	103	-6.4
40					51	+ 13					12	-33					73	-33

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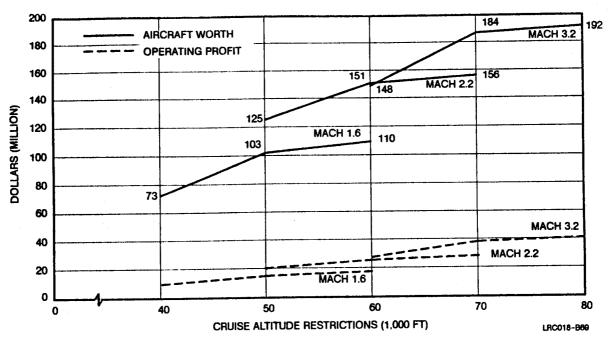


FIGURE 5-14. EFFECT OF CRUISE ALTITUDE RESTRICTIONS ON AIRCRAFT WORTH AFTER COMMENCEMENT OF PRODUCTION (WITHOUT RESIZING)

aircraft. Both the Mach 2.2 and Mach 3.2 configurations result in considerably higher ozone depletions, especially in the out-years when production is in full swing. The accuracy of this result, however, is contingent on the accuracy of the Lawrence Livermore 2-D atmospheric model.

- Of the three engine concepts studied at Mach 3.2, the turbine-bypass engine creates the smallest ozone impact. This is largely a function of its low fuel burns resulting from high-performance characteristics. Although the variable-stream-control engine has lower EINO_x values, it burns considerably more fuel than the turbine-bypass engine and consequently has a greater impact on the ozone column.
- The above-mentioned results indicate the importance of considering all aspects of engine emissions and not just the $EINO_x$.
- The introduction of cruise altitude restrictions was shown to alleviate ozone impact for all Mach numbers except 3.2. At Mach 3.2, the increased fuel burn more than offset the advantage of lowering the injection altitude and resulted in an increase in ozone depletion.
- Restricting supersonic aircraft to an off-design lower cruise altitude will impose penalties
 on economic performance in the form of higher operating costs and, hence, reduced
 profits. These penalties are unlikely to be acceptable from a flight performance and economic standpoint. Therefore, any altitude restrictions must be established prior to the
 final Mach number selection and aircraft development stage.

5.6 FUTURE PLANS AND RECOMMENDATIONS

• The two most pressing needs in the engine emissions and ozone study area are improving the global atmospheric models and developing low-NO_x combustors. The prediction of

annual fuel burns from HSCT fleets can be considered to be a fairly mature process. The wide variation in ozone concentration results from the various atmospheric models clearly needs to be addressed before the intricacies of fleet sizes, flight paths, etc. can be meaningfully addressed by the airframers.

- There is an urgent need for well-defined emissions criteria. Trade studies, such as those conducted in this study, are valuable inasmuch as they can identify trends and rule out scenarios that are clearly unacceptable. However, before the final design and Mach number selection for an HSCT can be made, emissions criteria must be defined so that costly redesigns and delays can be avoided.
- Three-dimensional atmospheric models may become an industry standard if their accuracy proves to be superior to two-dimensional models and the computer costs are not excessive. To support three-dimensional models, it will be necessary to revamp current methodologies for generating global scenarios.
- It would be mutually beneficial if a standardized methodology and format were defined and followed by industry and university researchers.
- Current HSCT emissions scenarios do not adequately account for the effect of the subsonic fleet. This can be misleading with regard to data interpretation and may be causing significant error in the overall ozone results. The optimum solution to this problem would be for the airframers to agree on a representative subsonic fleet for the time period in question, and then include these emissions in the total HSCT predictions.
- Along with the commercial subsonic fleet, prediction accuracy would be improved by including military flights. Difficulties arise when eastern European countries are brought into consideration because flight data are difficult to obtain. Some effort, however, should be made to incorporate as much of the current aviation activity as possible so that sound decisions regarding engine emissions can be made for both supersonic and subsonic aircraft.
- The impact of traffic seasonality should be included in the development of engine emissions scenarios. The global transport and atmospheric chemistry have a seasonal dependence, as does the air traffic. These factors need to be addressed to determine their impact on overall ozone concentration results.
- Certain routes have the potential to be rerouted to avoid flights through regions that are
 thought to be particularly sensitive to ozone depletion. For example, transatlantic flights
 might be rerouted away from the typical polar routes if this proved to be beneficial from
 an ozone standpoint. Alternative emissions scenarios simulating these types of rerouting
 can be developed and sent to global modelers for assessment.

SECTION 6 CONCLUSIONS

Following are conclusions drawn from the system studies in the environmental, marketing, economic, and emission impact areas:

- Long-term prospects for international passenger traffic gains are good. Supersonic traffic demands are promising.
- World demands for new passenger aircraft, including supersonic transports, are showing healthy growth. HSCT projections for the year 2025 could total 2,300 aircraft. However, accurate HSCT fleet forecasts will require a better understanding of many complex factors such as elasticity, stimulation, fare premium, and supersonic cruise overland restrictions.
- Supersonic operation may introduce major changes to the current global route structure to avoid overland flights. With creative rerouting, some supersonic network scenarios show good potential of capturing half the long-range markets.
- The atmospheric impact model results of vertical ozone depletion show a significant dependence on cruise injection altitude.
- Ozone depletion is significantly less with the Mach 1.6 configuration than with the Mach 2.2 and Mach 3.2 configurations for a given combustion technology.
- The introduction of cruise altitude restrictions after production implementation alleviates ozone impact for all Mach numbers except 3.2. At Mach 3.2, the increased fuel burn more than offset the advantage of lowering the injection altitude and resulted in an increase in ozone depletion.
- Restricting supersonic aircraft to an off-design lower cruise altitude will impose penalties on economic performance in the form of higher operating costs and, hence, reduced airline operating profits. The penalties are unlikely to be acceptable from a flight performance economic standpoint. Therefore, any altitude restrictions must be established prior to final Mach number selection in the aircraft development stage.

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SECTION 7 RECOMMENDATIONS

Following are the recommendations for the environmental, marketing, economic, and emission impact areas:

- Continue market and economic analysis of HSCT commercial value and economics, considering fuel prices, operational procedures, dispatch reliability, and environmental concerns.
- Continue parametric studies of different design ranges and passenger configurations to optimize the HSCT's economic viability.
- Continue supersonic network research on ways to respond to environmental concerns, operational policies, marketing strategies, and airline requirements.
- Continue to assess the effect of these supersonic network scenarios on aircraft economic performance, productivity, and fleet projections.
- In atmospheric emission impact, continue Mach number trade studies after (1) twodimensional atmospheric models have been updated to include fine grid densities and the effects of heterogeneous chemistry and (2) the city-pair network has been updated.
- Use three-dimensional atmospheric models for baseline atmospheric impact scenarios and compare the results to the two-dimensional model data.
- Future effects of HSCT operation on ozone depletion should include the effects of the subsonic fleet in the atmosphere for an appropriate year (e.g., 2015).
- Consider the effects of including additional subsonic operation (e.g., military, USSR, China, cargo, and turboprop).
- Evaluate the effects of traffic seasonality on atmospheric effects.
- Develop alternative emission scenarios to avoid routes having high sensitivity to ozone depletion (e.g., rerouting of polar routes).

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APPENDIX A BASIC TRAFFIC DATA BASE 250 CITY-PAIRS IN DESCENDING ORDER OF SCHEDULED SEATS

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4 T O O O D T	CITY	DIST	TATA		AIRCRAFT		AIRCRAF	т	DEPTS	ACM	SFAT	HOUR	ASM
AIRPORT CODES	CITY				MILES	SEATS	HOURS	ASMS000					
HNL-LAX	HNL-LAX	2551	12	154	392854	46351	790	118242	1	1	1	1	3
JFK-LHR	NYC-LON	3441	3	97	333777	33591	620	115584	2	2	2	4	4
HNL-NRT	HNL-TYO	3813	10	79	301227	32377	634	123453	4	4	3	3	1
HNL-SFO	HNL-SFO	2394	12	83	198702	24597	409	58886	3	6	4	5	8
LAX-NRT	LAX-TYO	5440	10	58	315520	22570	658	122782	5	3	5	2	2
FRA-JFK	FRA-NYC	3844	3	46	176824	15763	390	60595	8	7	6	6	7
NRT-SFO	TYO-SFO	5112	10	41	209592	15524	381	79360	9	5	7	7	5
NRT-SIN	TYO-SIN	3324	18	41	136284	15450	280	51355		13	8	12	11
BKK-NRT	BKK-TY0	2881	18	46	132526	15142	275	43624	7	14	9	13	16
CDG-JFK	PAR-NYC	3623	3	48	173904	15048	354	54521	6	8	10	9	9
FCO-JFK	ROM-NYC	4264	3	29	123656	12104	264	51612		16	11	15	10
JFK-MXP	NYC-MIL	3983	3	28	111524	11949	217	47592		19	12	20	13 18
GIG-MIA	RIO-MIA	4172	1	33	137676	9872	275	41187		12	13	14 10	6
JFK-NRT	NYC-TYO	6727	10	24	161448	9220	333	62024		10 11	14 15	11	29
BRU-JFK	BRU-NYC	3655	3	38	138890	8971	313 375	32790 41776		9		8	17
NRT-SVO	TYO-MOW	4659	9	37	172383	8967	170	36648		45		42	23
HNL-OSA	HNL-OSA	4093	10	20	81860	8954 8736	216	47523		17		21	15
LAX-LHR	LAX-LON	5440	3	21	114240 78716	8713	156	31175		51	19		34
JFK-MAD	NYC-MAD	3578	3	22 21	76398	8596		31173		53			33
EWR-ORY	NYC-PAR AMS-NYC	3638 3632	3	26	94432	8499		30868		30		23	35
AMS-JFK LHR-YYZ	LON-YYZ	3544	3	23	81512	8428		29868		46			
JFK-TLV	NYC-TLV	5663	3	18	101934	8403		47585		23			
	SIN-SYD	3908	18	21	82068	8390		32787		44			
SIN-SYD NRT-SEA	TYO-SEA	4757	10	20	95140	8004		38075		29			
SIN-TPE	SIN-TPE	2012	18	22	44264	7806		15705		117			97
HNL-SEL	HNL-SEL	4538	10	24	108912	7763		35228		20			
LHR-SIN	LON-SIN	6757	9	19	128383	7595		51319		15		16	12
LHR-ORD	LON-CHI	3939	3	21	82719	7574		29833		42	29	33	42
NRT-SYD	TYO-SYD	4863	18	19	92397	7345		35718		32	30	37	25
ANC-NRT	ANC-TYO	3426	10	26	89076	7340		25145		35		29	53
BOM-LHR	BOM-LON	4479	9	20	89580	7213		32310		33	32	28	31
EWR-LGW	NYC-LON	3472	3	18	62496	7152		24832	54	66	33	72	54
BOS-LHR	BOS-LON	3254	3	21	68334	6979	134	22710	26	59	34	61	63
JFK-ZRH	NYC-ZRH	3919	3	21	82299	6954	162	27252	36	43	35	48	50
AKL-HNL	AKL-HNL	4403	11	20	88060	6875	163	30271	40	39	36	47	39
FRA-ORD	FRA-CHI	4328	3	26	112528	6760	244	29257	18	18	3 37	17	44
HNL-SYD	HNL-SYD	5074	11	20	101480	6642	201	33701	44	24	38		
LAX-LGW	LAX-LON	5463	3	17	92871	6614	178	36133	63	31			
LAX-SEL	LAX-SEL	59 56	10	17	101252	6428	222			2			
HNL-ORD	HNL-CHI	4235	12	21	88935	6181	169	2617	7 33	36	5 41		
JFK-SNN	NYC-SNN	3072	3	17	52224	6139	105	18860	62	88	3 42		
BKK-SYD	BKK-SYD	4684	18	15	70260	6069	131			58			
IAD-LHR	WAS-LON	3665	3	17	62305	6019				68			
DFW-FRA	DFW-FRA	5125	3		107625	5978				2			
JFK-MEX	NYC-MEX	2090	2	21	43890	5943				12			
FRA-IAD	FRA-WAS	4067	3		85407	5936				41			
FRA-HKG	FRA-HKG	5694	9	14	79716	5908				49			
NRT-YVR	TYO-YVR	4663	10		88597	5851				3			
LHR-SFO	LON-SFO		3		74914	5719				5			
HKG-SF0	HKG-SF0	6898	10		96572	5670				2			
ATL-LGW	ATL-LON				88536	5495				3			
PER-SIN		2428			36420	5458							
LAX-SYD	LAX-SYD	7490	11	14	104860	5446	6 208	4078	9 87	2	2 5	+ C	¢ 13

AIRPORT CODES	CITY -		IATA		AIRCRAFT MILES	CEATC	AIRCRAFT				SEAT		
		(311)				SEATS	HOURS	ASMS000	KANK	RANK	RANK	RANK	RANK
BKK-FRA	BKK-FRA	5570	9	13	72410	5409	156	30132	98	57	55	50	40
HNL-SEA	HNL-SEA	2675	12	21	56175	5404	114	14456	34	79	56	87	108
BKK-LHR	BKK-LON		9	13	77064	5377	161	31877	100	52	57	49	32
ATH-JFK	ATH-NYC		3	12	59028	5179	123	25475	108	72	58	70	52
DFW-LGW	DFW-LON		3	21	99834	5145	197	24460	28	26	59	26	55
LHR-NRT	LON-TYO		9	14	83356	5124	165	30509	88	41	60	45	38
DXB-LGW	DXB-LON		8	16	54352	5123	123	17404	65	84	61	71	79
CPH-SEA	CPH-SEA		3	20	96980	4900	196	23761	42	27	62	27	58
DEL-FRA	DEL-FRA		9	13	49413	4891	114	18590	101	98	63	85	73
FRA-NRT	FRA-TYO		9	13	75582	4821	145	28030	103	54	64	56	46
BKK-DXB	BKK-DXB	3032	19	19	57608	4811	118	14587	46	75	65	79	105
GIG-JFK	RIO-NYC	4800	1	13	62400	4792	123	23002	104	67	66	73	62
JFK-LGW CDG-YMX	NYC-LON	3459	3	14	48426	4785	97	16551	85	103	67	110	83
MEL-SIN	PAR-YMQ	3444	3	17	58548	4775	127	16445	60	73	68	64	86
HKG-YVR	MEL-SIN HKG-YVR	3752	18	13	48776	4684	103	17574	107	101	69	99	77
BOS-FRA	BOS-FRA	6368 3657	10 3	14	89152	4669	165	29732	83	34	. 70	44	43
DME-KHV	MOW-KHV	3812	9	14 21	51198	4655	100	17023	76	91	71	102	80
LIM-MIA	LIM-MIA	2620	1	19	80052 49780	4634	182	17665	30	48	72	32	75
ATL-FRA	ATL-FRA	4600	3	14	64400	4608	103	12072	51	94	73	98	129
NRT-ORD	TYO-CHI	6257	10	12	75084	4550 4435	121 138	20930	73	64	74	75	67
LHR-YMX	LON-YMO	3251	3	14	45514	4305	99	27750 13996	119	55	75	60	47
LHR-TLV	LON-TLV	2229	8	12	26748	4252	57	9479	91	112	76	108	110
BKK-FC0	BKK-ROM	5495	9	10	54950	4248	118	23344	117	237	77	222	173
KWI-LHR	KWI-LON	2897	8	12	34764	4215	83	12210	129	81	78	80	60
JNB-LHR	JNB-LON	5634	7	11	61974	4197	138	23646	116	156	79	136	124
CPH-JFK	CPH-NYC	3843	3	15	57645	4162	126	15995	123 68	70 74	80	58	
LAX-OGG	LAX-OGG	2481	12	14	34734	4123	74	10229	86	157	81	66	93
LHR-PHL	LON-PHL	3533	3	14	49462	4123	112	14567	89	97	82 83	154	159
AMS-YYZ	AMS-YYZ	3720	3	14	52080	4118	112	15319	70	90	84	90	106
BAH-LHR	BAH-LON	3160	8	14	44240	4103	101	12965	74	118	85	89	101
LCA-LHR	LCA-LON	2035	8	18	36630	4078	89	8298	56	148	86	101 129	116 207
LAX-TPE	LAX-TPE	6770	10	10	67700	4077	138	27601	135	61	87	59	48
ANC-SEL	ANC-SEL	3769	10	13	48997	4060	114	15302	97	100	88	84	102
DFW-SJU	DFW-SJU	2163	2	14	30282	4060	66	8782	77	185	89	178	192
BKK-KHI	BKK-KHI	2299	18	13	29887	4008	65	9215	99	189	90	182	178
BKK-SEL	BKK-SEL	2294	18	14	32116	4000	72	9176	75	175	91	157	179
FRA-YYZ	FRA-YYZ	3939	3	14	55146	3990	119	15716	81	80	92	78	96
CDG-IAD	PAR-WAS	3848	3	17	65416	3986	144	15339	58	62	93	57	100
BRU-ORD	BRU-CHI	4145	3	19	78755	3980	175	16497	47	50	94	36	84
DXB-FRA	DXB-FRA	3006	8	14	42084	3955	9 9	11887	79	124	95	107	130
EZE-MIA	BUE-MIA	4409	1	13	57317	3951	117	17421	102	77	96	82	78
GIG-MAD	RIO-MAD	5058	5	16	80928	3948	154	19967	66	47	97	52	70
BGI-JFK	BGI-NYC	2091	2	17	35547	3923	85	8203	57	154	98	133	210
PER-SYD	PER-SYD	2035	18	23	46805	3923	90	7983	22	108	99	128	221
DEL-LHR	DEL-LON	4180	9	10	41800	3911	91	16349	131	125	100	123	89
GUA-LAX	GUA-LAX	2193	2	19	41667	3910	95	8574	49	126	101	117	198
CCS-JFK	CCS-NYC	2115	1	19	40185	3836	90	8113	48	131	102	125	216
FRA-SIN	FRA-SIN	6383	9	9	57447	3771	111	24072	148	76	103	91	57
CDG-TLV	PAR-TLV	2041	8	17	34697	3738	75	7629	59	158	104	152	233
HKG-LGW	HKG-LON	5991	9	9	53919	3724	124	22310	149	85	105	67	64
MAD-MIA	AIM-DAM	4413	4	10	44130	3686	89	16267	137	119	106	131	90
LHR-SEA	LON-SEA	4783	3	9	43047	3680	87	17601	156	123	107	132	76
OSA-SIN	OSA-SIN	3069	18	11	33759	3639	68	11168	126	164	108	172	150

AIRPORT CODES	CITY	DIST (SM)		DEPTS	AIRCRAFT MILES	SEATS	AIRCRAF HOURS	T ASMSOOO			SEAT RANK		
AMS-ATL	AMS-ATL	4388	3	13	57044	3611	123	15845	96	78	109	68	95
IAH-LGW	HOU-LON	4840	3	14	67760	3500	127	16940	84	60	110	65	81
DME-IKT	MOW-IKT	2604	9	21	54684	3444	120	8967	29	83	111	76	187
CDG-NRT	PAR-TYO	6027	9	10	60270	3435	118	20703	130	71	112	81	68
OGG-SFO	OGG-SFO	2335	12	14	32690	3409	66	7960	92	173	113	180	222
DX8-KUL	DXB-KUL	3434	19	12	41208	3366	84	11558	114	127	114	134	134
BOM-SIN	BOM-SIN	2435	18	12	29220	3359	60	8179	110	199	115	203	213
BOM-FRA	BOM-FRA	4079	9	9	36711	3288	80	13412	141	147	116	141	112
HNL-LAS	HNL-LAS	2757	12	9	24813	3243	50	8941	150	257	117	262	189
LHR-NBO	LON-NBO	4248	7	9	38232	3235	79	13742	155	143	118	146	111
ORD-ZRH	CHI-ZRH	4428	3	14	61992	3172	123	14047	94	69	119	74	109
	WAS-TYO	6736	10	6	40416	3168	84	21340	299	129	120	135	66
IAD-NRT		2960	8	9	26640	3142	58	9298	153	241	121	218	175
JED-LHR	JED-LON HNL-MNL	5290	10	9	47610	3138	90	16599	151	104	122	127	82
HNL-MNL JFK-LIS	NYC-LIS	3357	3	12	40284	3109	81	10333	115	130	123	138	157
AKL-LAX	AKL-LAX	6512	11	8	52096	3093	96	20141	157	89	124	111	69
ORD-SJU	CHI-SJU	2072	2	14	29008	3080	65	6382	93	204	125	187	279
CVG-ORY	CVG-PAR	4144	3	12	49728	3048	100	12631	112	96	126	103	119
HNL-IAH	HNL-HOU	3896	12	7	27272	3038	49	11836	243	229	127	264	132
AUH-SIN	AUH-SIN	3672	19	8	29376	3018	56	11082	162	198	128	223	151
HNL-STL	HNL-STL	4120	12	7	28840	3017	55	12430	247	208	129	234	122
BKK-CPH	BKK-CPH	5344	9	10	53440	3010	115	16085	128	86	130	83	92
LGW-MIA	LON-MIA	4429	4	11	48719	3001	109	13292	124	102	131	94	113
	PAR-FDF	4266	4	8	34128	2957	72	12614	164	162	132	158	121
CDG-FDF				7	39382	2928	77	16473	184	134	132	149	85
ATH-SIN	ATH-SIN	5626	9		54712	2920	123	11412	72	82	134	69	141
ARN-JFK	STO-NYC	3908 5652	3 3	14 9	50868	2903	102	16408		92	135	100	87
CDG-LAX FRA-JNB	PAR-LAX	5396	3 7	8	43168	2901	96	15653	168	122	136	114	98
	FRA-JNB	6474	10	10	64740	2901	120	18781	133	63	137	77	72
HKG-SEA	HKG-SEA		10	7	44660	2900	93	18502		115	138	120	74
DTW-NRT	DTT-TYO	6380 3978	19	7	27846	2884	56	11473	189	222	139	224	138
BAH-HKG	BAH-HKG	3144	8	7	22008	2884	48	9067	190	283	140	266	183
BAH-LGW GUM-HNL	BAH-LON GUM-HNL	3797	10	13	49361	2884	94	10950		99	141	118	153
LHR-MIA	LON-MIA	4414	4	7	30898	2884	65	12730		180	142	186	118
AMS-LAX	AMS-LAX	5562	3	8	44496	2864	92	15930		116	143	121	94
JFK-MUC	NYC-MUC	4028	3		52364	2837	104	11427		87	144	96	139
BOS-SNN	BOS-SNN	2885	3		20195	2807	40	8099		300		304	218
BOS-LGW	BOS-LON	3272	3	7.	22904	2800	46	9162		275		281	180
LGW-MSP		4022	3	7.	28154	2800	63	11262		219		194	146
OSA-SFO	LON-MSP OSA-SFO	5374	10	7	37618	2800	68	15047		144		171	104
	SEA-SEL				36260	2800	80	14504			149		
SEA-SEL		5180				2793	42	7211		295		299	
DEL-SIN	DEL-SIN	2582	18		20656 36616	2758	78	12624				147	120
CDG-MIA	PAR-MIA	4577		8				9891		253		256	
CGK-NRT	JKT-TYO	3623			25361	2730 2730	51	8657				217	196
HNL-NAN	HNL-NAN	3171	11		28539		58			213			
AMS-ORD	AMS-CHI	4106			32848 47070	2724 2713	69 94	11185 12770		169 105		165 119	117
LHR-YVR	LON-YVR	4707											
LGW-NRT	LON-TYO	5967			35802 46783	2706 2700	72 96	16148 11482		153 109		159 116	91 136
JFK-WAW	NYC-WAW	4253			46783 39767	2667	80	15151		133		142	
FRA-SFO	FRA-SFO	5681	3		50568	2665	110	11230		93		92	
DUS-ORD	DUS-CHI	4214			45133	2665	100	10935				104	154
HEL-JFK	HEL-NYC	4103				2625	74	9510		152		153	
JFK-ORY	NYC-PAR	3623			36230		103	10001		111			
BCN-JFK	BCN-NYC	3820	3	12	45840	2618	103	10001	109	111	102	3/	103

AIRPORT	CITY	DIST	IAŤA		AIRCRAFT		AIRCRAF	T	DEPTS	S ACM	SEAT	HOUR	ASM
CODES	CODES				MILES	SEATS	HOURS	ASMS000	RANK	RANK	RANK	RANK	
CMB-DXB	CMB-DXB	2043	19	12	24516	2610	52	5332	111	260	163	252	321
CDG-PTP	PAR-PTP	4204	4	7	29428	2583	56	10858	203	197	164	226	155
AMS-YMX	AMS-YMQ	3429	3	7	24003	2576	51	8834	181	266	165	255	191
BAH-FRA	BAH-FRA	2755	8	9	24795	2559	54	7051	140	258	166	238	255
KUL-MEL	KUL-MEL	3946	18	6	23676	2559	45	10097	302	268	167	288	161
SFO-TPE	SFO-TPE	6439	10	10	64390	2544	131	16381	138	65	168	63	88
DEN-HNL	DEN-HNL	3347	12	10	33470	2530	70	8468	132	167	169	163	199
AKL-SIN	AKL-SIN	5222	18	9	46998	2525	96	13184	139	107	170	112	115
MEL-NAN	MEL-NAN	2401	18	8	19208	2516	39	6040	173	311	171	322	290
EZE-MAD	BUE-MAD	6257	5	6	37542	2487	69	15564	290	145	172	168	99
HKG-SYD	HKG-SYD	4581	18	6	27486	2480	54	11361	297	227	173	243	144
KHV-VKO	KHV-MOW	3823	9	7	26761	2450	. 79	9366	251	236	174	145	174
LED-TAS	LED-TAS	2102	9	7	14714	2450	34	5150	254	391	175	367	331
UUS-VKO	UUS-MOW	4146	- 9	7	29022	2450	100	10158	269	202	176	106	160
HKG-MEL	HKG-MEL	4601	18	6	27606	2442	54	11238	296	226	177	242	147
AUH-CGK	AUH-JKT	4101	19	7	28707	2414	55	9897	188	212	178	230	164
BRU-YMX	BRU-YMQ	3461	3	9	31149	2409	67	8338	143	178	179	173	205
BOS-CDG	BOS-PAR	3436	3	9	30924	2404	59	8260	142	179	180	208	208
CCS-MAD	CCS-MAD	4349	4	9	39141	2398	75	10429	144	139	181	151	158
AMS-DXB	AMS-DXB	3208	8	7	22456	2384	48	7648		279	182		
AMS-AUA	AMS-AUA	4893	4	8	39144	2362	80	11556	158				
PEK-SHJ	BJS-SHJ	3609	19	8	28872	2345	71	8464		207	184		200
FRA-PEK	FRA-BJS	4836	9	6	29016	2343	59	11331					
KHI-PEK	KHI-BJS	3003	18	9	27027	2325		6983					
BOS-ZRH	BOS-ZRH	3732	3	7	26124	2319		8654					
LGW-YYZ	LON-YYZ	3564	3		39204	2299		8194					
AMS-IAH	AMS-HOU	4998	3		34986	2296		11475					
DME-HTA	MOW-HTA	2937	9		41118	2296		6744					
UUD-VKO	UUD-MOW	2758	9		38612	2296		6332					
HNL-PHX	HNL-PHX	2910	12		17460	2286		6652					
FRA-MIA	FRA-MIA	4820			43380	2277		10976					
DXB-MNL	DXB-MNL	4290			25740	2256		9678					
EWR-LHR	NYC-LON	3454	3		24178	2240		7737					
JFK-MAN	NYC-MAN	3330			23310	2240		7459					
HAV-YQX	HAV-YQX	2345			16415	2212		5187					
BKK-OSA	BKK-OSA	2601	18		18207	2209		5747					
CNS-NRT	CNS-TYO	3653			21918	2206		8060					
AKL-NRT	AKL-TYO	5490			32940	2202		12090					
GVA-JFK	GVA-NYC	3852			26964	2196		8459					
JIB-RUN	JIB-RUN	2392			11960	2179							
KUL-NRT	KUL-TYO	3337			26696	2156							
MAD-MEX	MAD-MEX	5631			28155	2150							
HNL-SAN	HNL-SAN	2609			18263	2114							
DXB-ZRH	DX8-ZRH	2959			17754	2113 2071							
FRA-YMX	FRA-YMQ	3647			25529 28470	2063							
FCO-GIG	ROM-RIO	5694			49752	2003							
MIA-SCL	MIA-SCL	4146				2037							
BOG-JFK	BOG-NYC	2481			17367	2030							
HNL-SJC	HNL-SJC	2413			16891	2025							
DXB-HKG	DXB-HKG	3694				2025							
HKG-LHR	HKG-LON	5989			17536	2024							
CAI-LHR	CAI-LON	2192				2024							
HNL-NGO	HNL-NGO	4006				2015							
AMS-DHA	AMS-DHA	2946	6 6	, 6	1/0/0	£01.	, 50		.,.				

AIRPORT	CITY	DIST	IATA		AIRCRAFT		AIRCRAF	T	DEPTS	S ACM	SEAT	HOUR	ASM
CODES	CODES	(SM)	CODE	DEPTS	MILES	SEATS	HOURS	ASMS000	RANK	RANK	RANK	RANK	RANK
	DUC 14V	5671			34026	2007	68	11381	287	163	217	170	143
DUS-LAX	DUS-LAX BOM-HKG	2670	3 18		16020	1998	34	5335		370	217	361	320
BOM-HKG	AMS-BOS	3445	3		24115	1988	54 54	6849	_	265	219	237	261
AMS-BOS	BOS-GLA	3020	3		21140	1988	43	6004	195	287	220	294	292
BOS-GLA CDG-DTW	PAR-DTT	3948	3	-	27636	1988	61	7849		225	221	199	224
DTW-FRA	DTT-FRA	4147	3		29029	1988	57	8244		201	222	220	209
		4224	3		46464	1988	96	8398	121	110	223	115	204
JFK-VIE	NYC-VIE ANC-SFO		12	14	28196	1974	63	3975		217	224	190	394
ANC-SFO	MNL-RUH	2014 4831	19	_	24155	1965	47	9493	_	264	225	279	171
MNL-RUH	CAI-LON	2171	8		13026	1920	31	4168		427	226	387	385
CAI-LGW		5942	5		29710	1919	60	11405		192	227	205	142
FRA-GIG	FRA-RIO		4		32718	1909	68	8924		172	228	169	190
AMS-PBM	AMS-PBM FDF-PAR	4674 4255	4	4	17020	1908	32	8120		352	229	378	215
FDF-ORY			-		16772	1908	32	8000		358	230	386	220
ORY-PTP	PAR-PTP	4193	4	4 5	19225	1900	35	7306		310		358	
HND-HNL	TYO-HNL	3845			18480	1895	39	5835		321	232	321	300
LHR-RUH	LON-RUH	3080	_		22110	1891	48	6967		282	233	267	258
DEL-FCO	DEL-ROM	3685	_	_	24630	1889	48	7756		259	233	271	226
LAX-PPT	LAX-PPT	4105 4786		_	33502	1883	62	9012		166			186
ATL-MUC	ATL-MUC				26832	1883	54	8422		234			203
BNE-NRT	BNE-TYO	4472			30429	1883	57	8185		184	237	219	
CVG-FRA	CVG-FRA	4347		-	27783	1883	53	7474		224			239
CVG-LGW	CVG-LON	3969		-	33670	1883	61	9057		165			185
NRT-PDX	TYO-PDX	4810				1883	81	9890					
PDX-SEL	PDX-SEL	5252			36764 29888	1877	65	7012		188		-	
DUS-JFK	DUS-NYC	3736					38	6492					_
BOS-BRU	BOS-BRU	3468			20808	1872 1870	46	8688					
JFK-SVO	NYC-MOW	4646			23230	-							
KHG-SHA	KHG-SHA	2592			18144	1869	15	4844					
MAD-SDQ	MAD-SDQ	4154			29078	1862	56	7735					
GIG-LHR	RIO-LON	5746			28730	1857	55	10670		211	246		
FRA-YVR	FRA-YVR	5007			40056	1856	82	9293					
FRA-THR	FRA-THR	2339			16373	1833	36	4288					
DPS-MEL	DPS-MEL	2726			19082	1830	37	4988					
DTW-SEL	DTT-SEL	6603	10	4	26412	1800	58	11885	386	242	250	214	131

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APPENDIX B GREAT CIRCLE VERSUS DIVERTED DISTANCES STRIP CHARTS FOR TOP 20 CITY-PAIRS

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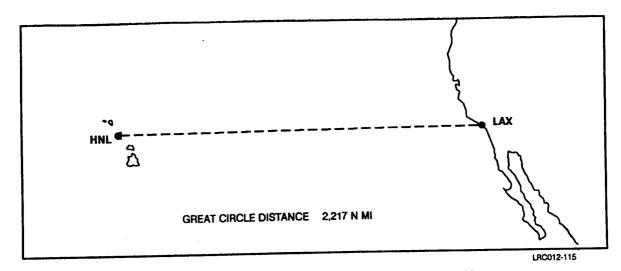


FIGURE B-1. HSCT ROUTE CHART FOR HNL-LAX

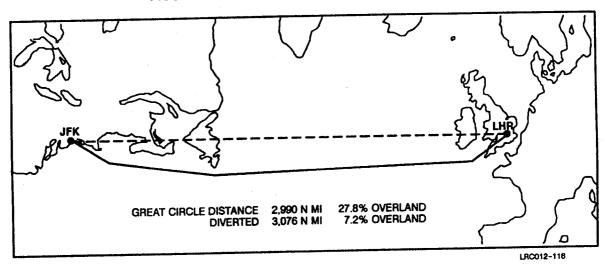


FIGURE B-2. HSCT ROUTE CHART FOR JFK-LHR

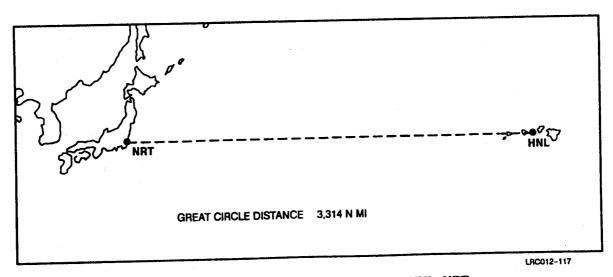


FIGURE B-3. HSCT ROUTE CHART FOR HNL-NRT

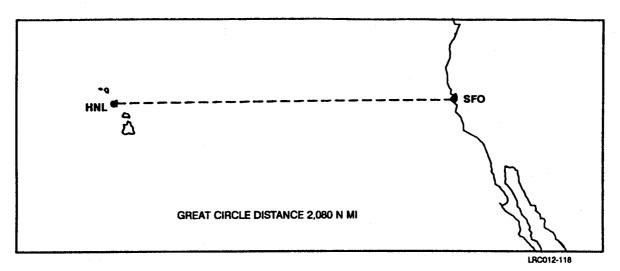


FIGURE B-4. HSCT ROUTE CHART FOR HNL-SFO

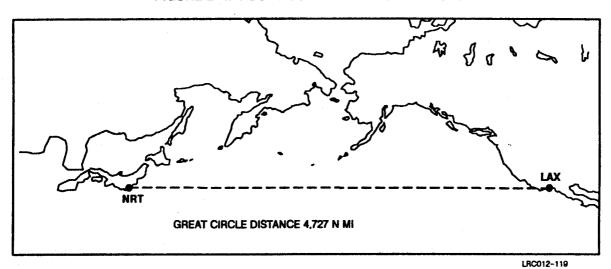


FIGURE B-5. HSCT ROUTE CHART FOR LAX-NRT

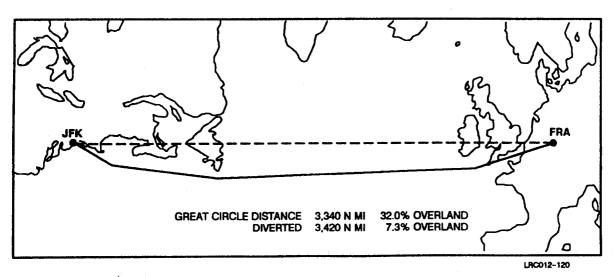


FIGURE B-6. HSCT ROUTE CHART FOR FRA-JFK

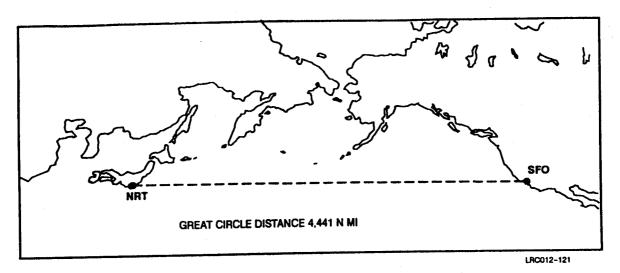


FIGURE B-7. HSCT ROUTE CHART FOR NRT-SFO

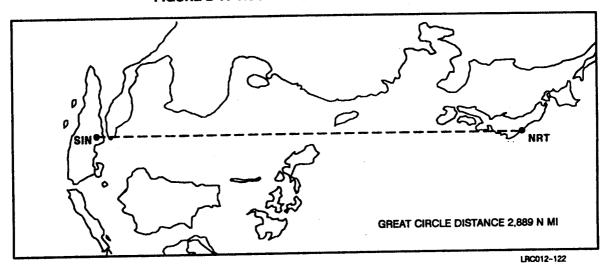


FIGURE B-8. HSCT ROUTE CHART FOR NRT-SIN

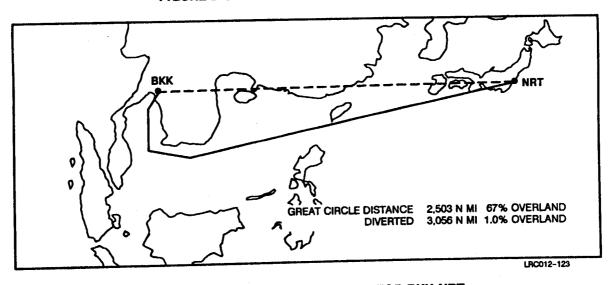


FIGURE B-9. HSCT ROUTE CHART FOR BKK-NRT

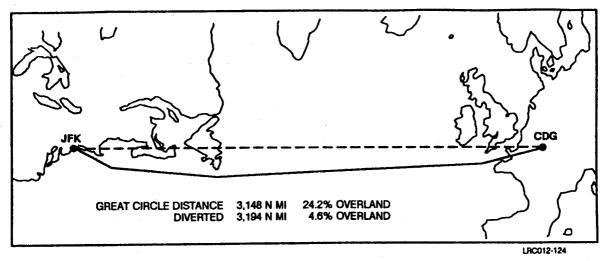


FIGURE B-10. HSCT ROUTE CHART FOR CDG-JFK

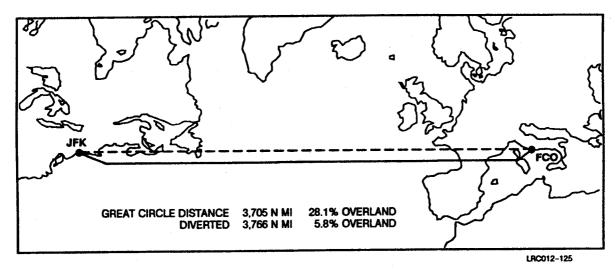


FIGURE B-11. HSCT ROUTE CHART FOR FCO-JFK

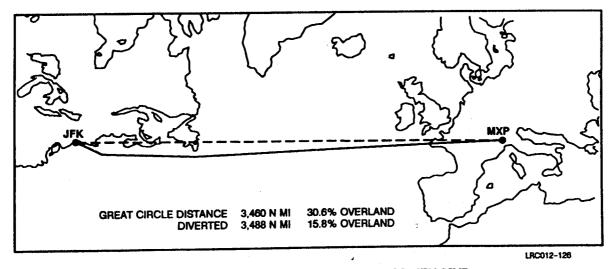


FIGURE B-12. HSCT ROUTE CHART FOR JFK-MXP

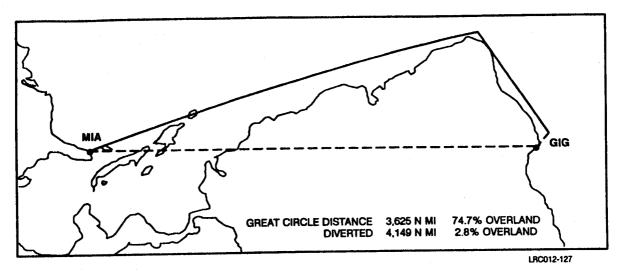


FIGURE B-13. HSCT ROUTE CHART FOR GIG-MIA

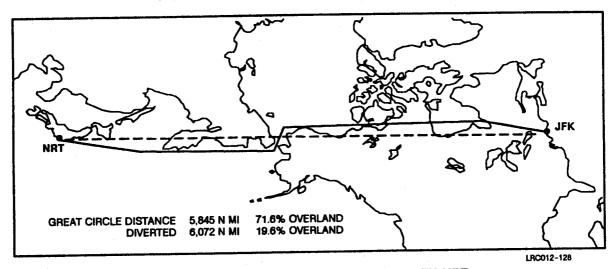


FIGURE B-14. HSCT ROUTE CHART FOR JFK-NRT

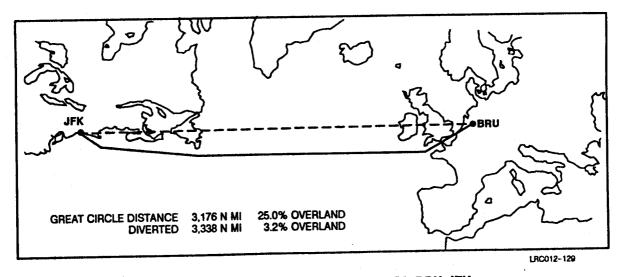


FIGURE B-15. HSCT ROUTE CHART FOR BRU-JFK

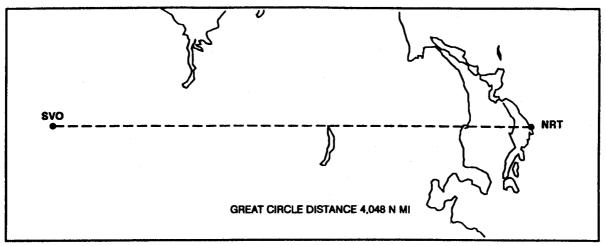
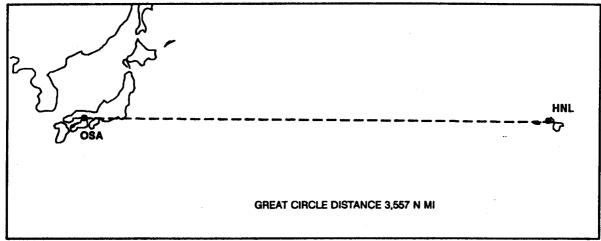


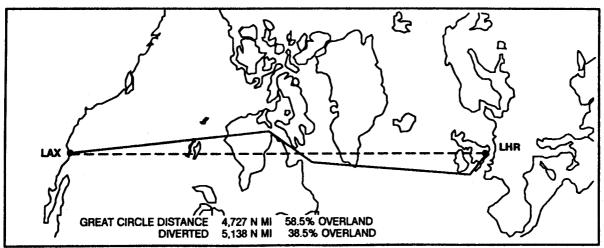
FIGURE B-16. HSCT ROUTE CHART FOR NRT-SVO

LRC012-130



LRC012-131

FIGURE B-17. HSCT ROUTE CHART FOR HNL-OSA



LRC012-132

FIGURE B-18. HSCT ROUTE CHART FOR LAX-LHR

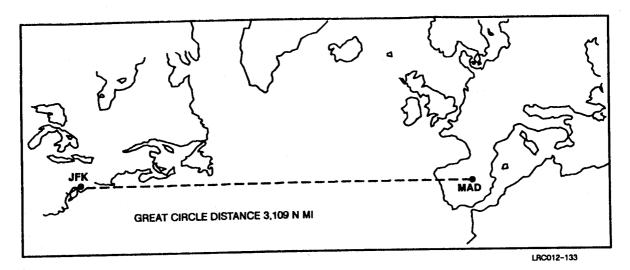


FIGURE B-19. HSCT ROUTE CHART FOR JFK-MAD

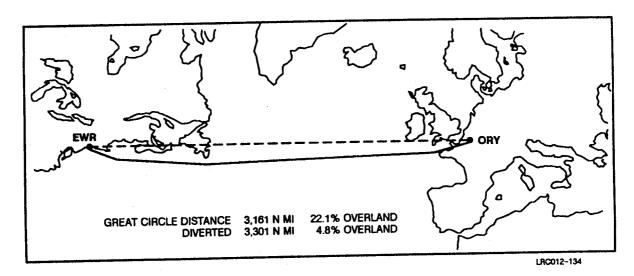


FIGURE B-20. HSCT ROUTE CHART FOR EWR-ORY

,			

APPENDIX C GROUND TRACK PROFILE DISPLAY 250 CITY-PAIRS

•		

Primary Sort: Overland %

														6	iround	l Trac	k Len	ath :	X			1
	ATRPORT	ΙΔΤΔ	RT	DIST	GC Range	0ver1	and	Divert	ed ()verlan	Cum	1	1 2					-	7 8	3 9		0
*		CODE			(N.Mi.)		*	Range	Dist	×		0 () () () () () ()	0 0) (0 (0
	HNL-LAX*			2551	2217	0	0.0	2217	0	0.0	0.00	 			اا				 	ļ		!
2	HNL-NRT*	10	1	3813	3314	0	0.0	3314	0	0.0	0.00	[[• • • •				!
3	HNL-SFO*	12	1	2394	2080	0	0.0	2080	0	0.0	0.00					• • • • •		• • • •				ļ
	LAX-NRT*			5440	4727	0	0.0	4727	0	0.0	0.00						• • • • •	• • • •	• • • •	• • • • 		
	NRT-SFO*			5112	4441	0	0.0	4441	0	0.0	0.00		!					• • • •		• • • •		!
	NRT-SIN*			3324	2889	0	0.0	2889	0	0.0	0.00							• • • •		• • • • } 		!
	SIN-SYD*			3908	3360	1892	56.3	5364	0	0.0								• • • •		• • • • 	ļ	
	SIN-TPE			2012	1748	0	0.0	1748 4592	0	0.0 0.0	0.00	1	• • • •	· · · · 				• • • •		i		1
	HNL-SEL			4538	3944	181 0	4.6 0.0	3826	0	0.0	0.00	1	· · · · ·	• • • • : 	· · · · 					1	l	i
	AKL-HNL			4403 5074	3826 4409	66	1.5	4416	0	0.0	0.00								i	i	i	i
	HNL-SYD'			5956	5175	0	0.0	5175	0	0.0	0.00		· · · · ·	i					i	i	i	i
	LAX-SEL* BKK-SYD*		-	4684	4070	2389	58.7	5649	0	0.0	0.00		 	:						i		i i
	HKG-SF0		_	6898	5994	851	14.2	6181	0	0.0	0.00	i	i	i	i		i i	i	i	İ	i	i i
_	LAX-SYD		-	7490	6508	0	0.0	6508	0	0.0	0.00	i	i	i	i	i	i		i	İ	j	Ì.
	GIG-JFK			4800	4171	1852	44.4	4796	0	0.0	0.00	i				i			j	j	j	i.
	LAX-OGG	12	_	2481	2156	0	0.0	2156	0	0.0	0.00	İ	i	j	İ		j	İ	j	İ	İ	Ì٠
	PER-SYD			2035	1768	1360	76.9	2302	0	0.0	0.00	i	İ	j	j	j	İ	Ì	İ	j	ĺ	.
	BGI-JFK			2091	1816	0	0.0	1816	0	0.0	0.00	j	j				 	١	1	1	1	.
	CCS-JFK'		1	2115	1837	0	0.0	1837	0	0.0	0.00	1	1	1	1	 	 	١	1	 	1	.
21	OSA-SIN'	18	1	3069	2667	0	0.0	2667	0	0.0	0.00	1	 	 	 	l		ļ	ļ		ļ	.
22	OGG-SFO	12	1	2335	2029	0	0.0	2029	0	0.0	0.00	ļ	ļ	ļ	ļ	ļ		ļ	ļ		ļ	٠ [.
23	BOM-SIN'	18	1	2435	2115	632	29.9	3601	0		0.00	ļ		ļ					1	1		.
24	HNL-MNL'	. 10	1	5290	4597	0	0.0	4597	0		0.00	ļ	ļ			ļ						٠
25	JFK-LIS	3		3357	2917	0	0.0	2917	0		0.00		ļ	ļ					ļ			٠
	AKL-LAX			6512	5685	0	0.0	5685	0		0.00			• • • •						····		·
_	HKG-SEA			6474	5588	1743	31.2	5907	0		0.00				ļ			· · · ·			1	:
	GUM-HNL'			3797	3300	0	0.0	3300	0		0.00			1		· · · ·] · · · ·			1	1
	BOS-SNN			2885	2507	521	20.8	2548 4556	0		0.00	1	• • • •			· · · ·			1	ļ	1	1
	SEA-SEL	10		5180	4501	900	20.0	4566 2755	0		0.00		····	! · · · ·		1]]	1		1	ï
	HNL-NAN			3171	2755	0 466	0.0 14.8	3245	0		0.00	·····	····	1			l		l	l	1	Ϊ
	CGK-NRT	18		3623 3946	3148 3429	2500	72.9	4782	0		0.00	1				1		i	İ	i		
	KUL-MEL	18 10 *		6439	5596	716	12.8	5633	0		0.00	i	····	ļ	i	 			i	i	j	i.
	SFO-TPE' AKL-SIN			5222	4556	1904	41.8	4867	0		0.00	i	ì	i		i		j	j	İ	İ	i.
	MEL-NAN			2401	2086	309	14.8	2255	0		0.00	İ	i	i	j	i	j	j	. j	j	j	٠Ĺ
	HKG-SYD	18		4581	3983	2410	60.5	4497	0		0.00	j	İ	j	j	j	j	Ì	. j	1	. j	٠ĺ
	AMS-AUA			4893	4252	272	6.4	4278	0	0.0	0.00	į	1	ĺ	1	1	1	1	.	 		١.
	AMS-IAH		1	4998	4343	2662	61.3	5055	0	0.0	0.00	1	1	1	 	1	1	ļ	.	ļ		٠ إ
40	CNS-NRT	1 8	1	3653	3174	225	7.1	3435	0		0.00		1	•	•	•	•	•	. 	•	. 	
41	AKL-NRT	* 18	1	5490	4771	. 0	0.0	4771	0	0.0									. .			
42	KUL-NRT	* 18	1	3337	2900	0	0.0	2900	0	0.0	0.00	 	ļ	ļ	ļ	ļ	ļ	ļ	.		.	.]
43	HNL-SAN	12	1	2609	2267	0	0.0	2267	0	0.0	0.00	ļ	ļ	ļ	ļ	ļ	ļ	ļ	.	· • • • •	.	٠ļ
44	FCO-GIG	* 5	1	5694	4984	2367	47.5	5330	0		0.00	ļ		ļ		ļ		ļ	. 	ļ	· · · ·	-
45	HNL-SJC	12	1	2413	2096	0	0.0	2096	0										.			
	HNL-NGO			4006		0	0.0	3481	0		0.00			ļ	1				.		.	-
	BOS-GLA			3020		585	22.3	2693	0			1		ļ	1	1	1		٠	1	1	1
	AMS-BOS			3445		1266	42.3	3141	0		0.00	1	1	1	1	1	1		. .	1	1	1
	HND-HNL			3845		0	0.0		0			1	. [1	1	1	1	1	· · · · · .	1	1	1
-	LAX-PPT			4105		0	0.0		0		0.00	1	1	1	1	1	1	1	.	.	.]	1
	BNE-NRT			4472		323	8.3 8.6	3940 4606	0		0.00	1		1	1	1	1	1	.	.	.	i.
	PDX-SEL			5252		393 0	0.0		(0.00	1	. i	j	1	i	j	į	.	. j	.j	i.
	NRT-PDX			4810 2726		1421	62.8		Č			1		. j	ĺ	j	į	1	. j	. .	. İ	ا.
	DPS-MEL					1038	46.2		Č										. j			
5	JFK-KEF	* 3		2586	, (24/	1000	70.2	. 701	•			•	•	•	•	,		•	•			

Configuration: Mach 3.2-Subsonic Overland, 6Hr Curfew, 2hr Turnaround.

Primary Sort: Overland %

					Ground Track Length %									1									
		NT 1		ОТ	nter	GC Range	Overla	and	Divert	ed 0	verlan	Cum		1						7 8	3 9	9 '	0
					(SM)	(N.Mi.)	_	%	Range	Dist	x	×	0	0	0	0 (0	0	0 (0 () ()	0
# 66	NRT-S		18		4863	4226	1040	24.6	4388	22	0.5	0.04	1	.		 	ļ		ļ]			ļ
	BKK-N		18		2881	2503	1695	67.7	3056	31	1.0				:	:					• • • •		- *
	AMS-		3		3632	3156	814	25.8	3353	34	1.0	0.15	•	·	:	:	:	:	i		• • • •		* .
	JFK-1		3	1	5663	4921	2746	55.8	5178	52	1.0	0.23		.					•			· · · ·	*
60	JFK-	SNN*	3	1	3072	2669	544	20.4	2716	27	1.0	0.26	1	.			• • • •				· · · · 	i · · · ·	1
61	LAX-	TPE*	10	1	6770	5883	682	11.6	5898	59	1.0	0.32	Ţ	.]	1	ļ	1			 	! · · · · · 		1
62	LHR-I	*AIM	4	1	4414	3836	361	9.4	3842	85	2.2		- 1	.	1		1			ļ		l	*
63	JFK-	MAN*	3		3330	2894	1210	41.8	3030	70	2.3	0.50								Ì			*
64	BKK-	SEL*	18		2294	1994	1603	80.4	2816	68	2.4 2.4	0.50											*
	CMB-				2043	1776	455	25.6	1897	46 74	2.5	0.67		.						j			*
	BOS-				3254	2827	591	20.9	2956	108	2.6							•	•	j			*
	NRT-				4757	4133	174	4.2	4144 3340	87	2.6	0.83	*	1		Ì	i	j	j	j	İ	Ì	*
	DX8-				3434	2984	534 2708	17.9 74.7	4149	116	2.8	0.92	1	.i		1	1	.	.		1	1	.
	GIG-				4172		72	3.1	2325	72	3.1		j	. j	. j	j	. j	1	. '	**
	HNL-				2675		794	25.0	3338	107	3.2	1.04	. **			·
	BRU-				3655		935	29.3	3486	112	3.2	1.11	**		. .	.1	.1	.	.	.	ļ	.	.]
	AUH-		19		3672 3454		1324	44.1	3070	98	3.2	1.17	۱	٠إ	1	.	**
	EWR-				3272		847	29.8	2889	95	3.3		1	$\cdot \cdots $.	.	1	. '	**
	805- BOS-		_		3468		1338	44.4	3097	111	3.6	1.29) 	.1 			**
	5 HKG-		-		6368		2308	41.7	5832	216	3.7	1.41	.	.		.	٠	.	.	. ;	1,	.	
	7 MIA-				2 4146		1802	50.0	3945	150	3.8	1.49	 	$\cdot \cdot \cdots $. **.	.	.	. [• • • •	.	1	• • • •	• [
	B ANC-		12		2014		67	3.8	1750	67	3.8	1.52	· ** · ·	.		.	.	• • • •	-	.		٠	• [
	ATH-				2 4919		1607	37.6	4889	220	4.5	1.63	3	**		.]	• • • •	• • • •	• • • •	.		٠¦۰۰۰	- 1
	CDG-				1 3623		762	24.2	3194	147	4.6	1.70) ***.		$\cdot \cdots $	-	.	$\cdot \cdots$	-	.]	• • • •	• • • • •	·
	1 EWR-				3472		803	26.6	3183	146	4.6		' [···	··[···		• • • •	· · · · ï			.	• • • •	:	*
	2 AMS				1 4388	3812	1395	36.6	4157	191	4.6	1.8								$\cdot \cdots $			
	3 CDG			1	1 4577	3977	183	4.6	3977	183	4.6	1.93	3 ***]	.	-	.		.	-1	• 1 • • •		
	4 EZE			5	1 6257	5437	2409	44.3	5712	263		2.03	3		$\cdot \cdots$	$\cdot \cdots$.	.		.	·[···		
	5 GUA			2	1 2193	1905	1905	100.0	2111	99		2.0	7 **.	$\cdots \cdots$					-	.	٠, ١٠٠٠	-	**
	6 EWR			3	1 3638	3161	699	22.1	3301	158		2.17	2		-	-	-1					1	**
8	7 G1G	-MAD	* !	5	1 5058	3 4396	725	16.5		213		2.2	0	• • • • •		-[.		-	.	.i		
8	8 LGW	-MIA	* 4	4	1 4429	3849	362	9.4		185	_	2.2	b """		[. 1	**	-	1	1	.i	1	***
8	9 JFK	-MEX	* :	2	2 209			61 . 4		99		2.2	3 ··			1	1			.			1
9	O CPH	-JFK	•	3	1 384			23.7		169		2.3	• • •			1			.i	.j	.i	i	***
9	1 NRT	-YVR		-	1 466			7.1		208 192			7 **						. i	j	.j	j	*
_	2 AUH				1 410			36.2								i	. i	i		j			***
9	3 IAH	-LGW		-	1 484			57.1													.		***
-	4 GIG				1 574			26.9													.	:	***
-	5 JFK			_	1 362			22.0			-	2.7	1 i	İ	. 1		l				.		***
	6 BOS				1 343			21.: 28.				2.7	7	**	* 1	İ	1]
	7 FCO			3	2 426			29.				2.8	15 ***	1]]				
	8 FRA				1 594			6.	-			2 9	11 ***		1								
	9 MAD			4	1 441	_		47.				2 0	16 **	1									
	O LHR			3	1 382			13.				3.0	2 ***	٠		:.		$\cdots \cdots $!
	1 BCN			3	1 467						6 6.3	3.0	08 ***	٠					$\cdots \cdots$				
	2 AMS			4 3	1 373		·					3.1	13 ***	٠						$\cdot \cdot \cdot \cdot$		$\cdot \cdot \cdot \cdot$	
	03 DUS			4	1 434				- :		2 6.4	3.1	18	٠٠٠إ٠٠		$\cdots \cdots$		$\cdot \cdot \cdot \cdot$				•• ••	
	04 CCS 05 FR#			4	1 482	-					4 6.5	. 3	24 ***	*	1	1	1		[]	
	05 FKA 06 BKA			18	1 260		·				1 6.	5 3.	28 **					$\cdot \cdot \cdot \cdot$			•• ••		***
	DO DAY			2	1 234					7 13	9 6.8	3.3	31						$\cdots \cdots$		•••		
_	OB ATI			3	1 421					6 26	4 6.9	9 3.	37 **	· · · [· ·	• • • • • •								
	08 AII			1	2 26	-		_		7 18		9 3.	41 *.]		. TR.					[1	**
	10 MAI			4	1 563				.2 497	0 35	3 7.	1 3.	48 **	* .									• •
1	JU MAI	,-ML	r.	7																			

Secondary Sort: Seats Configuration: Mach 3.2-Subsonic Overland, 6Hr Curfew, 2hr Turnaround.

Primary Sort: Overland %

															(Srounc	! Trac	ck Le	ngth :	X		1
				nŦ	NICT	GC Range	Overla	and	Divert	ed 0v	erlan	Cum	1	. 2		3 4					8 9	
		AIRPORT CODES				(N.Mi.)	-	*	Range	Dist	×		0 0) (•	•	-		0 0
. 1					4255	3697	262	7.1	3697	262	7.1	3.54	1					ļ	ļ			.****
		FDF-ORY			3441	2990	831	27.8	3076	221	7.2	3.58	**					ļ	ļ	ļ		**
		JFK-LHR JFK-LGW		_	3459	2996	833	27.8	3082	222	7.2	3.63	**									*
					3844	3340	1069	32.0	3420	250	7.3	3.68	***			'			1			ļ <u>"</u>
		FRA-JFK			5374	3643	270	7.4	3643	270	7.4	3.73	****]	ļ	ļ		
		OSA-SFO HNL-OSA		-	4093	3557	263	7.4	3557	263	7.4	3.78	1				ļ		ļ		ļ	
					3429	2979	1341	45.0	3312	255	7.7	3.82	j] <u> </u>				ļ	.] · · · ·	ļ	ļ	****
		AMS-YMX			4193	4670	369	7.9	4670	369	7.9	3.89	****					ļ	. .			
		ORY-PTP BOS-FRA		-	3657	3178	953	30.0	3312	265	8.0	3.94				ļ	ļ <i>.</i>	ļ	.]	. ****
				_	3578	3109	255	8.2	3109	255	8.2	3.99	j		 	ļ		ļ	.	1	ļ	.***
		JFK-MAD			4266	3707	308	8.3	3707	308	8.3	4.05	****.		 	ļ	ļ	ļ	. 	ļ		[]
		CDG-FDF		_	3426		444	14.9	3031	255	8.4	4.09	****.		 	1	ļ		.	\ 	1	
-		ANC-NRT			4154	3609	303	8.4	3609	303	8.4	4.15	****	 	ļ	ļ	ļ	ļ	.	1	ļ	ļļ
		MAD-SDC	•		4204	3653	321	8.8	3653	321	8.8	4.21	****	 	 	ļ	J		· • · · · ·			1
		CDG-PTF			3848		883	26.4	3376	300	8.9	4,26	**	ļ	ļ	1	1	. [.		. [***
-		CDG-IA			4067		1428	40.4	3619	362	10.0	4.33	***.,	1]	1	ļ	.]	. [.	· [· · · ·	**
-	-	FRA-IA	•		3665		1271	39.9	3260	339	10.4	4.39	**	1		ļ	Į	.	$\cdot \cdots $	٠	٠ ٠ ٠ ٠ ٠	1***
		IAD-LH			1 3732		1281	39.5	3290	345	10.5	4.46	i	1	J	.J	[.	.	.	.	*****
		BOS-ZRI			1 3461		1320	43.9	3269	350	10.7	4.52	**	1	ļ	.]	1	٠	.	.	$\cdot \cdots $. .****
_		BRU-YM			3769		874	26.7	3417	372	10.9	4.59	****.	1	1	.	ļ *
		ANC-SE			1 2757		266	11.1	2395	266	11.1	4.64	i	1	\	.	1	*****
		HNL-LA		_	1 3908		1383	40.9	3536	392	11.1	4.71	****	1	1	.	1	
		ARN-JF		-	-		281	11.1	2529	281	11.1	4.76	3	1	1	.	1	٠ ٠ ٠ ٠	.	.	· : · · · ¹	*****
	-	HNL-PH		_	1 2910		1915	47.9	4179	485	11.6	4.8	5 **	1	1	
		ATL-FR	• •	-	1 4600 1 3969			53.5	3653	424	11.6	4.93	****	*	.1 "
		CVG-LG		-	1 325			42.9	3200	384	12.0	4.99	3 ***		***
		LHR-YM		-	1 372			49.1	3625	442	12.2	5.0	7	.	.1	.	.	$\cdot \cdot \cdot \cdot$.		*****
		AMS-YY	_	_	2 484			65.2	5074	624	12.3	5 1	R **	. 1	. 1		.			. ***	.	
		CPH-SE		-	_			37.3		400	12:5	5.2	5 ***.	. 1	.		.					
		CDG-YM		_	1 344			42.0		422	12.5	5.3	2 ****	***	
		GVA-JF		-	-			31.2		247	12.7	5.3	6 ****	*** [.[]
		DFW-SJ			1 216			74.4		759		5.4	8 *	.1	.	.	.1	$\cdot \cdots $. **	***		.1*
		LHR-NR		_	2 595			44.8		532		5 5	7	1	1	.1		.1			*	*****
		JFK-WA	_		1 425			48.4		493		5.6	5 ****	.1	. 1		.			.		
	-	FRA-YN		3	1 364			14.5			14.5		****	***	.1		.1					
		S PER-S		.8	1 242			62.1			14.6	5.8	1 ***.	.1	. j	.1	.1					*****
		6 ATL-MI		3	1 478			31.8				5.9	0 ***.	.1	.1		.					
		7 FRA-Y		3	1 393			43.8				5.0	g ****	***	1			1]] [
		B HEL-JI		3	1 410			83.3				6.1	3 *	.1	.]	1	.			. ****	**	
		9 LGW-NI		9	2 596			48.9			15.6	6.2	2 ****	****	.1	1]				[]
		O AMS-O		3	1 410						15.8	6.3	u 1	.1	.1	1					¹	****
		1 JFK-M		3	1 398			30.6			15.9	6.4	14 1	**	***	٠. [.*]]
		2 ATH-S		9	2 562			72.5					2 ****	***	1	: . 1						
		3 JFK-M		3	1 402			39.7				6.6	32 ****	**		1						
		4 CVG-F		3	1 434								72 ****	***	1						~ . }	••["•••]
		5 EZE-M		1	2 440							. 61	R6 *	. 1	. 1				. *	****	**	"
		6 FRA-N		9	2 58	-						. 6	96 ***	****								
		7 CVG-0		3	1 414							, ,	11 ***	**		****	l					
		8 DTW-N		10	2 63							. 7	97 ***1	**	1	****			1			
		9 DTW-S		10	2 66							7.	27	- 1	- 1	1	!]		""	*****
		O LGW-M		3	1 40							2 7	AC ***	****	- 1	1			1			
	16	1 CDG-D	WT	3	1 39							2 7	54 İ	- 1	1			1.				
		2 JFK-Z		3	1 39							2 7	59 ***	***	**			.				
	16	3 BOG-3)FK	1	1 24						8 18.	r 7	60 **	- 1	- 1	1] .	l .			
		64 BRU-C		3	1 41	45 360						U 1.	78 ***				ij	i .	İ .	İ		*****
		55 LGW-1		3	1 35	64 309	37 1505	5 48.	6 334	, 65	3 19.	J /.		1				•	•	•		

Configuration: Mach 3.2-Subsonic Overland, 6Hr Curfew, 2hr Turnaround.

Primary Sort: Overland %

												Ground Track Length % 1
	AIRPORT	ATA	RT	DIST	GC Range	Over	and	Divert	ted 0	verlan	Cum	1 2 3 4 5 6 7 8 9 0
	CODES	CODE	TYP	(SM)	(N.Hi.)	Dist	×	Range	Dist	*	*	0 0 0 0 0 0 0 0 0 0
166	JFK-NRT*	10	2	6727	5845	4185	71.6	6072	1190	19.6	7.94	
167	CDG-NRT*	9	2	6027	5237	4509	86.1	5607	1110	19.8		*
168	IAD-NRT	10	2	6736	5853	4624	79.0	6171	1271	20.6	8.25	
169	DTW-FRA	3	1	4147	3604	1971	54.7	3802	810	21.3	8.35	*********
170	JFK-SVO	3	1	4646	4037	2176	53.9	4198	924	22.0	8.47	
171	DUS-ORD*	3	1	4214	3663	1648	45.0	3988	897	22.5		· **
172	DFW-FRA*	3	1	5125	4453	2672	60.0	4807	1139	23.7		*********.
173	CDG-TLV*	8	1	2041	1773	1183	66.7	1859	446	24.0		**********
174	LHR-YYZ*	3	1	3544	3079	1512	49.1	3341	809	24.2	8.90	**** ***************************
175	JFK-VIE*	3	1	4224	3670	2007	54.7	3736	919	24.6		*********
176	FRA-YVR	3	1	5007	4351	3263	75.0	4671	1224	26.2		**********
177	JIB-RUN	16	1	2392	2078	547	26.3	2078	547	26.3	9.25	
178	LHR-SEA	3	1	4783	4156	3051	73.4	4746	1253	26.4		*
179	FRA-ORD*	3	1	4328	3761	1809	48.1	4055	1087	26.8		****
180	LHR-TLV*	8	1	2229	1937	1395	72.0	2383	670	28.1	9.64	
181	AMS-LAX	3	1	5562	4833	3025	62.6	5111	1452	28.4	9.83	
182	DEN-HNL	12	1	3347	2908	846	29.1	2908	846	29.1	9.93	
183	ORD-ZRH*	3	1	4428	3848	2213	57.5	4073	1250	30.7	10.10	
184	LHR-ORD*	3	1	3939	3423	1807	52.8	3702	1140	30.8		**
185	DFW-HNL*	12	1	3776	3281	1014	30.9	3281	1014	30.9		***************************************
186	LCA-LHR*	8	1	2035	1768	1660	93.9	2296	70 9	30.9		***********
187	NRT-ORD*	10	1	6257	5437	2876	52.9	5537	1744	31.5		
188	DFW-LGW*	3	1	4754	4121	2415	58.6	4279	1356	31.7	10.84	
189	LHR-YVR*	3	1	4707	4090	2597	63.5	4512	1430	31.7		***
190	HNL-IAH	12	1	3896	3385	1090	32.2	3385	1090	32.2		***********
191	FRA-SFO	3	1	5681	4937	3767	76.3	5204	1681	32.3		*
192	DUS-LAX	3	1	5671	4929	3283	66.6	5201	1774	34.1		5 **
193	CDG-LAX	3	1	5652	4912	2869	58.4	5132	1842	35.9	11.77	***************************************
194	ORD-SJU*	2	1	2072	1800	666	37.0	1800	666	37.0		5 *************************************
195	CAI-LHR	8	1	2192	1887	1408	74.6	1954	723	37.0		***********
196	CA1-LGW	8	1	2171	1905	1372	72.0	1972	730	37.0		***
197	LAX-LHR'	' 3	1	5440	4727	2765	58.5	5138	1978	38.5	12.26	
198	LAX-LGW	3	1	5463	4747	2777	58.5	5138	1978	38.5	12.49	
199	LHR-SF0	٠ 3	1	5351	4650	2646	56.9	5040	2016	40.0	12.73	
200	HNL-STL	12	1	4120	3580	1475	41.2	3580	1475	41.2	12.90	
201	HKG-MEL	18	1	4601	3998	1675	41.9	3998	1675	41.9	13.10	
202	HNL-ORD	* 12	1	4235	3680	1623	44.1	3680	1623	44.1	13.29	
203	DEL-SIN	18	1	2582	2243	998	44.5	2243	998	44.5	13.41	
204	KWI-LHR	* 8	1	2897	2517	2361	93.8	2762	1304		13.56	
	BKK-DXB			3032		1415	53.7	2635	1415		13.73	
206	MEL-SIN'	* 18	2	3752	3260	1757	53.9	3260	1757	53.9	13.95	5 *************************************
207	JED-LHR	8	2	2960	2572	1422	55.3	2572	1422	55.3	14.12	2
208	BKK-KHI	18	3	2299	1998	1451	72.6	1998	1451	72.6	14.31	******
209	LHR-NBO	7	3	4248	3691	2776	75.2	3691	2776	75.2	14.68	******
210	LHR-SIN'	* 9	3	6757	5872	4886	83.2	5872	4886	83.2	15.32	***************************************
211	MNL-RUH	19	3	4831	4199	3578	85.2	4199	3578	85.2	15.79	9 ************************
212	NRT-SVO	• 9	3	4659	4048	3663	90.5	4048	3663	90.5	16.27	7 **
	BOM-LHR		4	4479	3892	3892	100.0	3892			16.78	8 ***************
	FRA-HKG		4	5694	4948	4948	100.0	4948	4948	100.0	17.43	3 ****************
	BKK-FRA		4	5570	4389	4389	100.0	4389		100.0	17.99	9 **************
	BKK-LHR		4	5928	5151	5151	100.0	5151		100.0	18.64	4 *************************************
	DXB-LGW		. 4	3397	2952	2952	100.0	2952	2952	100.0	19.01	**************
	DEL-FRA		. 4	3801	3303	3303	100.0	3303		100.0	19.42	2 ***************
	DME-KHV			3812	3312	3312	100.0	3312	3312	100.0	19.82	2 ****************
	BKK-FC0			5495	4775	4775	100.0	4775	4775	100.0	20.40	0 ****************

Configuration: Mach 3.2-Subsonic Overland, 6Hr Curfew, 2hr Turnaround.

-															Gro	und	Track	Lengt	h %			1
				0167	CC D.===	0ver1	and	Divert	ed (Overlan	Cum		1	2	3	4	5	6	7	8	9	0
					GC Range (N.Mi.)		*	Range	Dist		4	0	0	0	0	0	0	0	0	0	0	0
		CODE			4896	4896	100.0	4896	_	100.0	20.98	****	***	****	****	***	****	****	***	****	*****	**
	JNB-LHR			5634 3160	2746	2746	100.0	2746	2746	100.0	21.30	***	***	****	****	***	****	****	****	****	*****	**
	BAH-LHR			3006	2612	2612	100.0	2612	2612	100.0	21.61	****	***	****	****	****	****	****	****	****	*****	**
	DXB-FRA			4180	3632	3632	100.0	3632	3632	100.0	22.03	****	***	****	****	****	****	*****	****	****	*****	k #
	DEL-LHR	* 9 9		6383	5546	5546	100.0	5546	5546	100.0	22.66	****	***	****	****	****	****	*****	****	****	*****	R#
	FRA-SIN HKG-LGW	9		5991	5206	5206	100.0	5206	5206	100.0	23.25	***	***	****	****	****	****	****	****	****	****	R#
	DME-IKT	-		2604	2262	2262	100.0	2262	2262	100.0	23.50	***	***	****	****	****	****	****	****	****	****	**
	BOM-FRA	9	-	4079		3545	100.0	3545	3545	100.0	23.89	****	***	****	****	***	*****	****	****	****	****	**
	BKK-CPH			5344		4644	100.0	4644	4644	100.0	24.39	****	***1	****	****	****	****	****	*****		****	**
	FRA-JNB	_		5396		4688	100.0	4688	4688	100.0	24.90	****	***	*****	****	***	*****	****	****	*****	****	**
	BAH-HKG			3978		3457	100.0	3457	3457	100.0	25.55	****	***1	*****	****	***	*****	****	****		*****	**
	BAH-LGW			3144		2732	100.0	2732	2732	100.0	25.19	****	***	****	****	***	****	****	****	*****	****	**
	BAH-FRA			2755		2394	100.0	2394	2394	100.0	25.80	****	***	****	****	***	*****	*****	****	*****	*****	**
	UUS-VKO			4146		3603	100.0	3603	3603	100.0	26.70	****	***	****	****	****	****	****	****	*****	*****	**
	KHV-VKO	_		3823		3322	100.0	3322	3322	100.0	26.34	****	***	****	****	****	****	****	****	*****	*****	***
	LED-TAS			2102		1827	100.0	1827	1827	100.0	25.99	****	***	****	****	***	****	****	*****	****	*****	
	AMS-DXB			3208		2787	100.0	2787	2787	100.0	26.99	****	***	****	****	***	****	*****	****	****	*****	***
	PEK-SHJ			3609		3154	100.0	3154	3154	100.0	27.30) ****	***	****	****	***	****	*****	****	****	*****	
	FRA-PE			4836		4202	100.0	4202	4202	100.0	27.72	2 ****	***	****	****	***	****	*****	****	****	*****	
	KHI-PE	•		3003		2610	100.0	2610	2610	100.0	27.98	B ****	***	****	***	***	*****		****		*****	
	UUD-VK			4 2758		2397	100.0	2397	2397	7 100.0	28.46	6 ****	***	****	****	****	*****	*****	****		*****	***
	DME-HT/			4 293		2552	100.0	2552	2552	2 100.0	28.23	3 ****	***	****	****	****	*****			*****	*****	***
	DXB-MNI		•	4 429	3728	3728	100.0	3728	3728	3 100.0	28.82	2 ****	***	****						****	******	***
	DXB-ZRI		3 4	4 2959	2571	2571	100.0	2571		1 100.0	29.06	6 ****	***	****	****	***	****		****	****	*****	***
_	HKG-LH		9 4	4 5989	5204	5204	100.0	5204		4 100.0	29.50	6 ****	***	****					****	****	*****	***
	DXB-HK		9 4	4 369	3210	3210	100.0	3210	321	0 100.0	29.8	6 ****	***	****	****		****		****	****	****	***
	AMS-DH		3 4	4 294	5 2560	2560	100.0	2560	-	0 100.0		9 ***	***	*****					****	****	*****	***
	BOM-HK		8 .	4 267	2320	2320	100.0	2320		0 100.0		1 ***	***	****					****	****	*****	***
	LHR-RU		В	4 308	0 2676	2676	100.0	2676		6 100.0		5 ***	****	****				*****	****	****	****	***
	DEL-FC		9 .	4 368	5 3203	3203	100.0	3203		3 100.0		4 ***	***					*****	****	****	*****	***
	KHG-SH	_	В	4 259	2 2252	2252	100.0	2252		2 100.0		5 ***	****	****				*****	****	****	****	***
	FRA-TH		В	4 233	9 2033	2033	100.0	2033	203	3 100.0	31.2	3 ***	****	*****				*****	****	****	****	***
	3 ABA-DM		9	4 209	4 1819	1819	100.0	1819	181	9 100.0	31.3	9 ***	***	****		****						
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REPORT DOCUMENTATION PAGE

Form Approved
OMB No. 0704-0188

Public reporting burden for this collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing this burden, to Washington Headquarters Services, Directorate for Information Operations and Reports, 1215 Jefferson Caule Highway, Suite 1204 Actionston, VA 22202-4302, and to the Office of Management and Budget, Paperwork Reduction Project (0704-0188), Washington, DC 20503.

Davis Highway, Suite 1204, Arlington, VA 22202-4302	2. REPORT DATE			
1. AGENCY USE ONLY (Leave blank)	DATES C	OVERED		
	October 1992	Contractor R		
4. TITLE AND SUBTITLE			5. FUNDI	NG NUMBERS
1990 High-Speed Civil T	ransport Studies			S1-18378 37-01-22-01
6. AUTHOR(S)				
HSCT Concept Developmen Advanced Commercial Pro				
7. PERFORMING ORGANIZATION NAME	(S) AND ADDRESS(ES)			RMING ORGANIZATION
McDonnell Douglas Corpor Douglas Aircraft Company 3855 Lakewood Boulevard Long Beach, CA 90846	y .		-	K0395-2
Long Beach, CA 70040		·		
9. SPONSORING/MONITORING AGENCY National Aeronautics an Langley Research Center Hampton, VA 23665-5225	d Space Administrat	· •	AGEN	SORING / MONITORING CY REPORT NUMBER CR-189618
		and the same of th		
11. SUPPLEMENTARY NOTES Langley Technical Monit Final Report	or: Donald L. Maid	len .	DOS BANGARIOS ANTO ART STEAMAR PA	
12a. DISTRIBUTION / AVAILABILITY STA	TEMENT		12b. DIST	TRIBUTION CODE
Unclassified - Unlimite				
Subject Category 05	a.			
nunlect category on				
		·		
13. ABSTRACT (Maximum 200 words)				
This report contains the related to High-Speed Contains of the system studies were design Mach numbers ranged and HSCT market and economics.	Civil Transports (HS of NASA Langley Reserve conducted to assessinging from 1.6 to 3. nomic assessment, de	CT's). The task earch Center Cont is the emission i 2. The tasks sp	s were ract N impact pecific	performed under AS1-18378. of HSCT's at ally addressed
and an atmospheric emis	ssions scenario.			
The general results ind traffic for the 2000 to and environmentally con supersonic overland tra land masses; and (3) th lower for Mach 1.6 oper	o 2025 time period t npatible HSCT's; (2) affic can be increas ne atmospheric emiss	to support a flee the HSCT route sed by innovative tion impact on or	et of e struct routi zone wo	conomically viable ure to minimize ng to avoid
14. SUBJECT TERMS				15. NUMBER OF PAGES
High-Speed Civil Transp	oort Systems Studies	3		81
Supersonic Transport				16. PRICE CODE
•				A05
17. SECURITY CLASSIFICATION 18. OF REPORT	SECURITY CLASSIFICATION OF THIS PAGE	19. SECURITY CLASSIFIC OF ABSTRACT	CATION	20. LIMITATION OF ABSTRACT
Unclassified	Unclassified	Unclassified		

Standard Form 298 (Rev. 2-89) Prescribed by ANSI 5td. 239-18 298-102